

Analysis and interpretation of the CFD results including a self-propulsion optimization

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Project Case

船体主尺度:

<u>Lpp</u> (m)	314.6
B(m)	52.5
T(m)	18.1
排水体积 (m ³)	253000

螺旋桨参数 Propeller:

Diameter (m)	9.6
P/D (0.7R)	0.74
Ratio	0.498

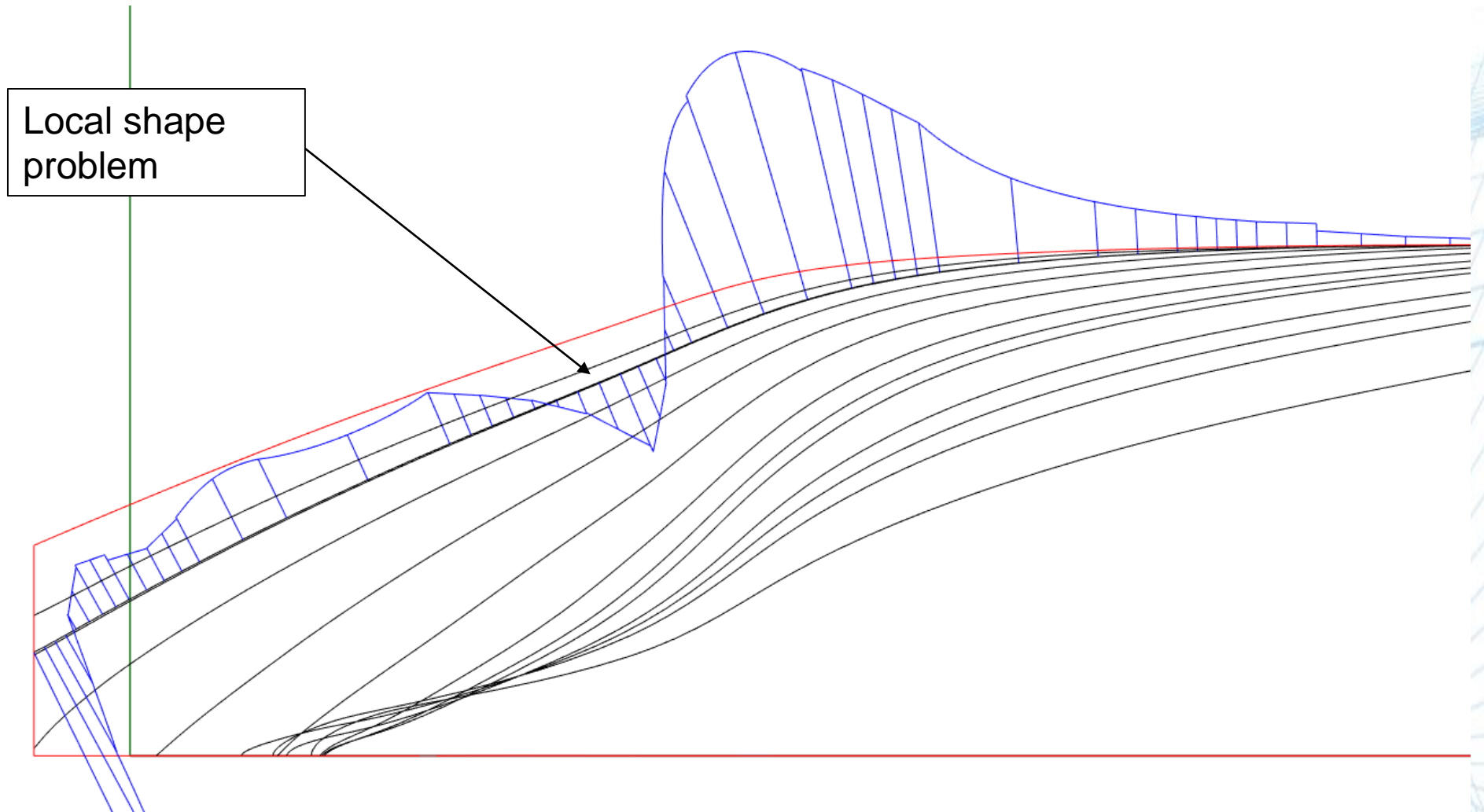


Tools

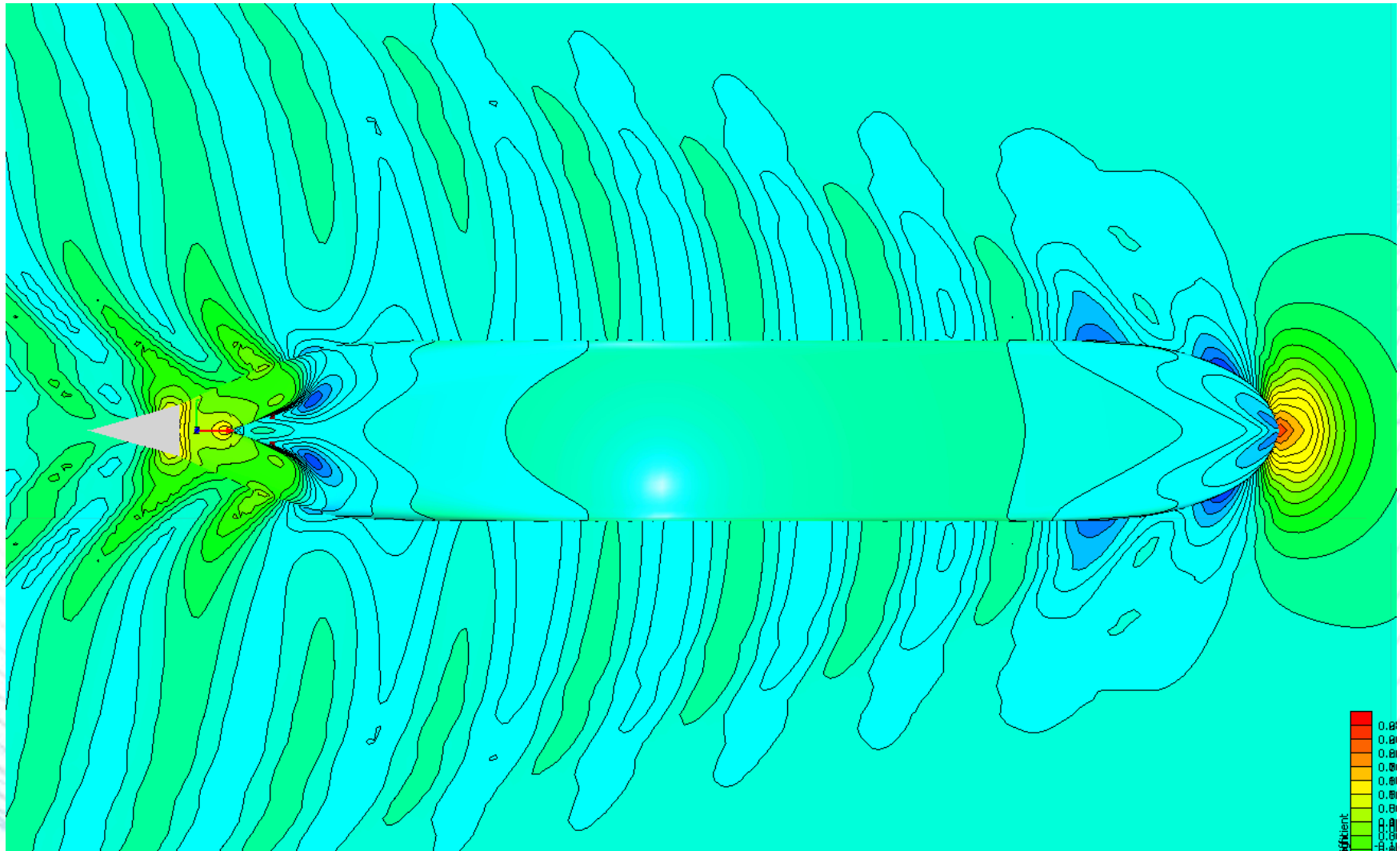
- Rhinoceros3d
 - hull inspection
 - initial corrections
- CAESES
 - hull transformations
 - optimization methods
 - postprocessing
- SHIPFLOW 6.5
 - CFD simulations (resistance, self-propulsion)

Initial hull evaluation

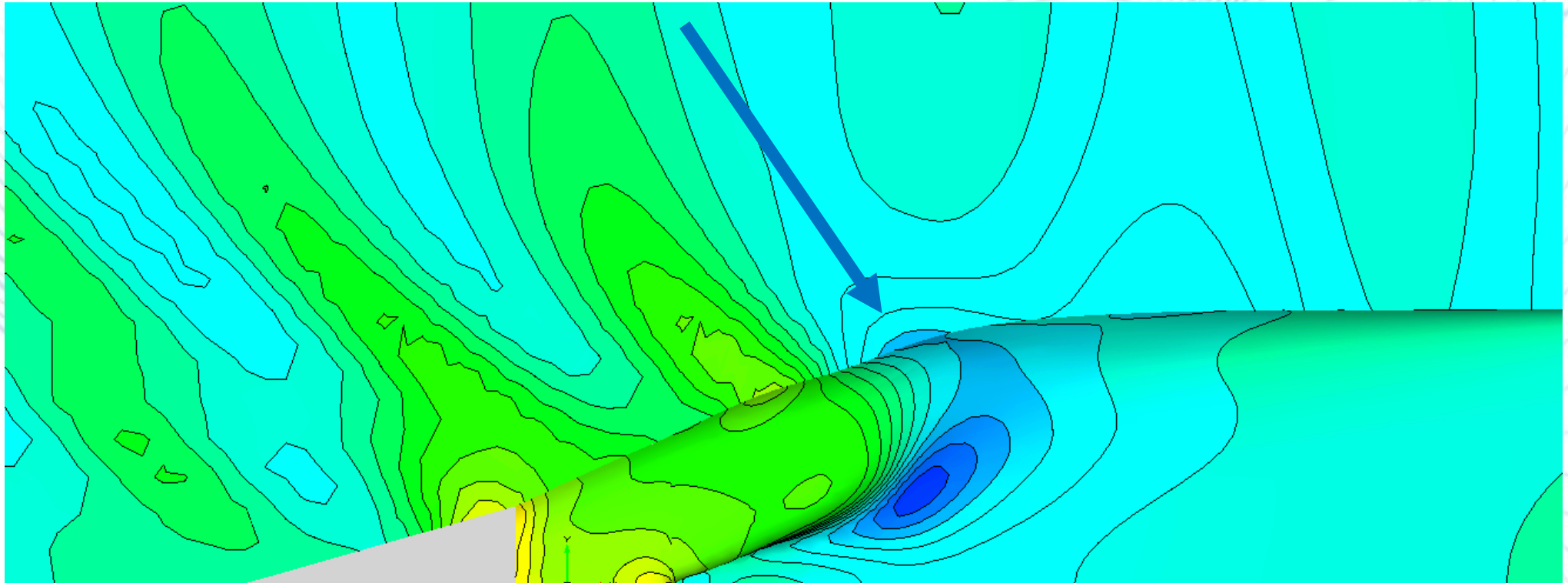
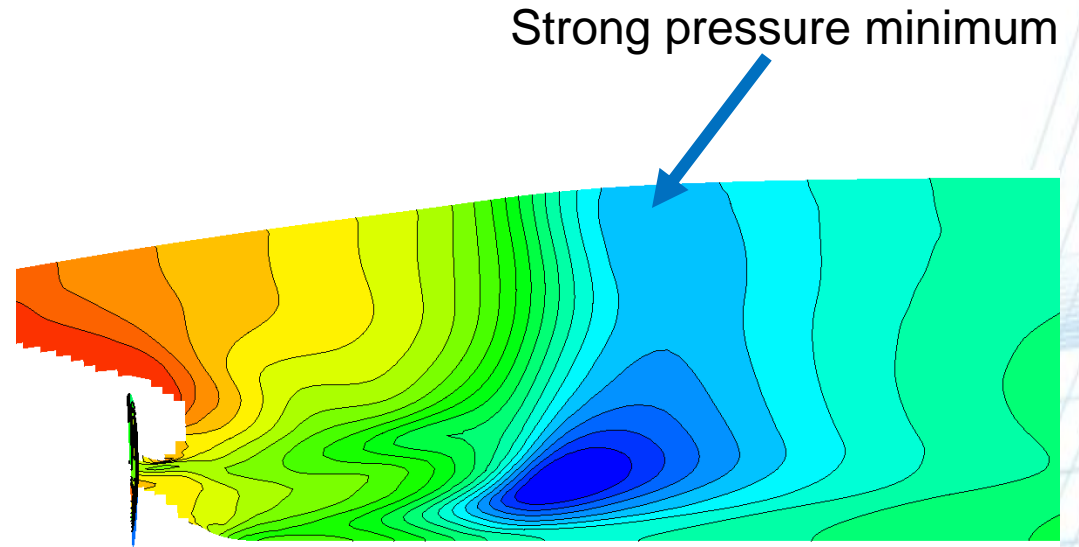
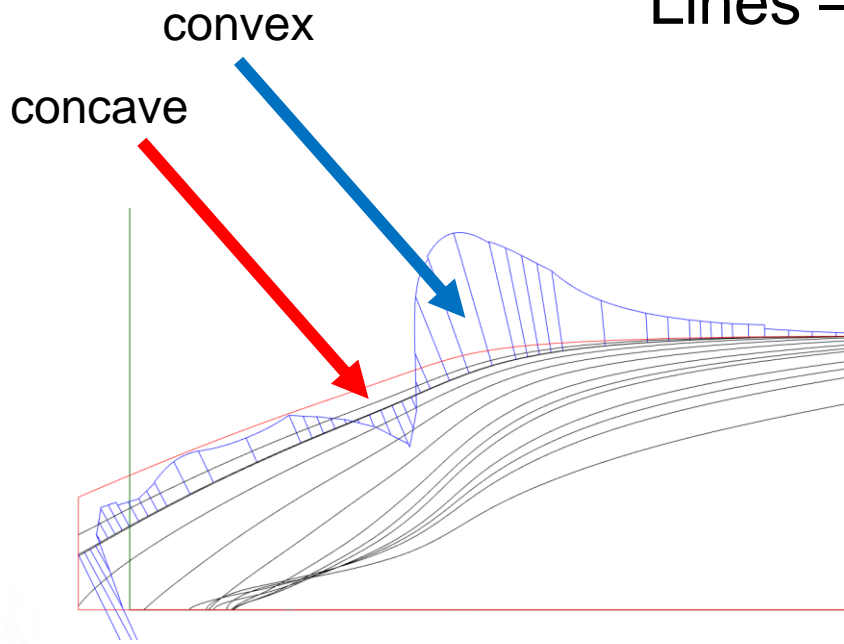
Hull Shape Inspection



Wave pattern and hull Cp distribution



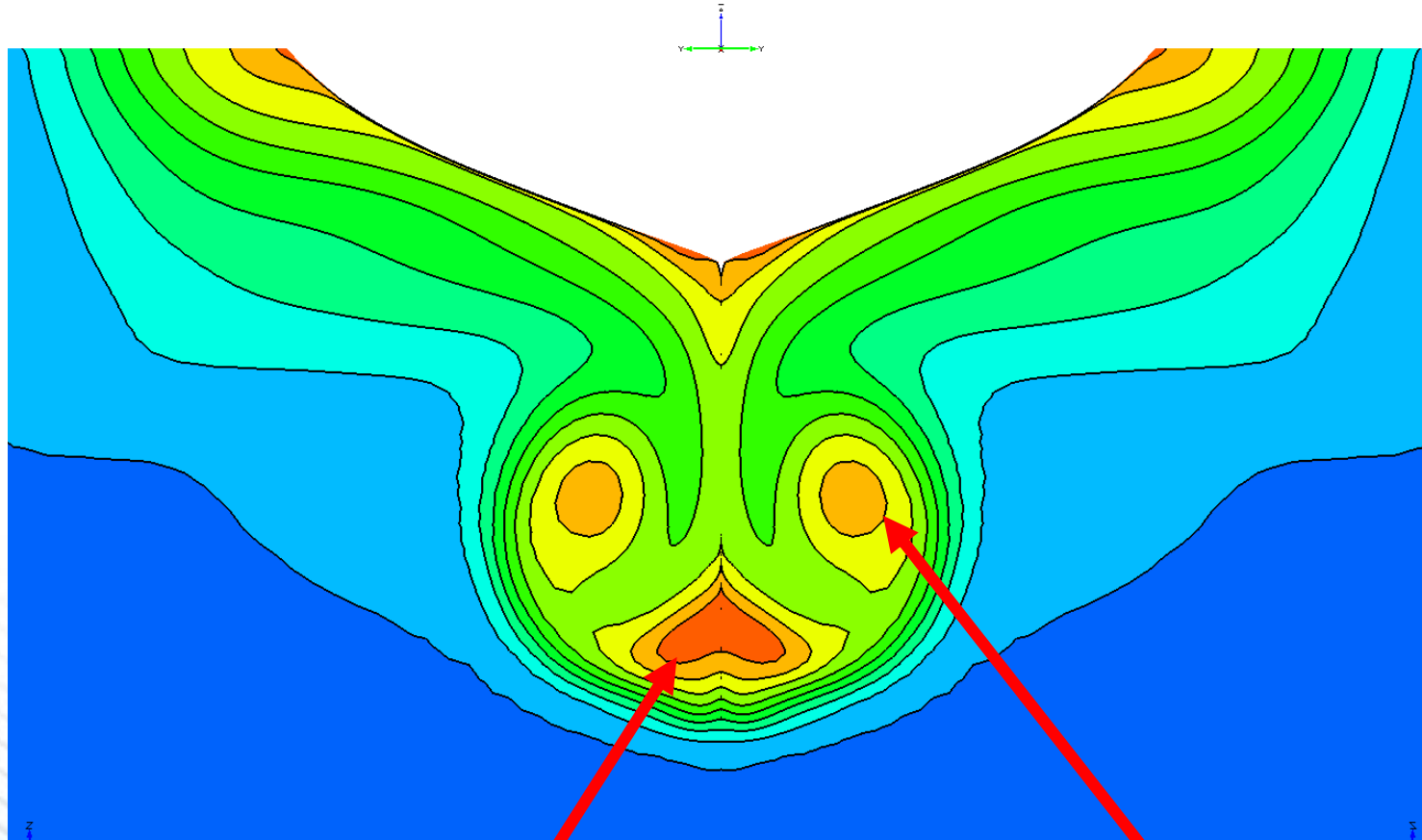
Lines – pressure correlation



WAVE RESISTANCE presentation: 2_

Viscous Flow

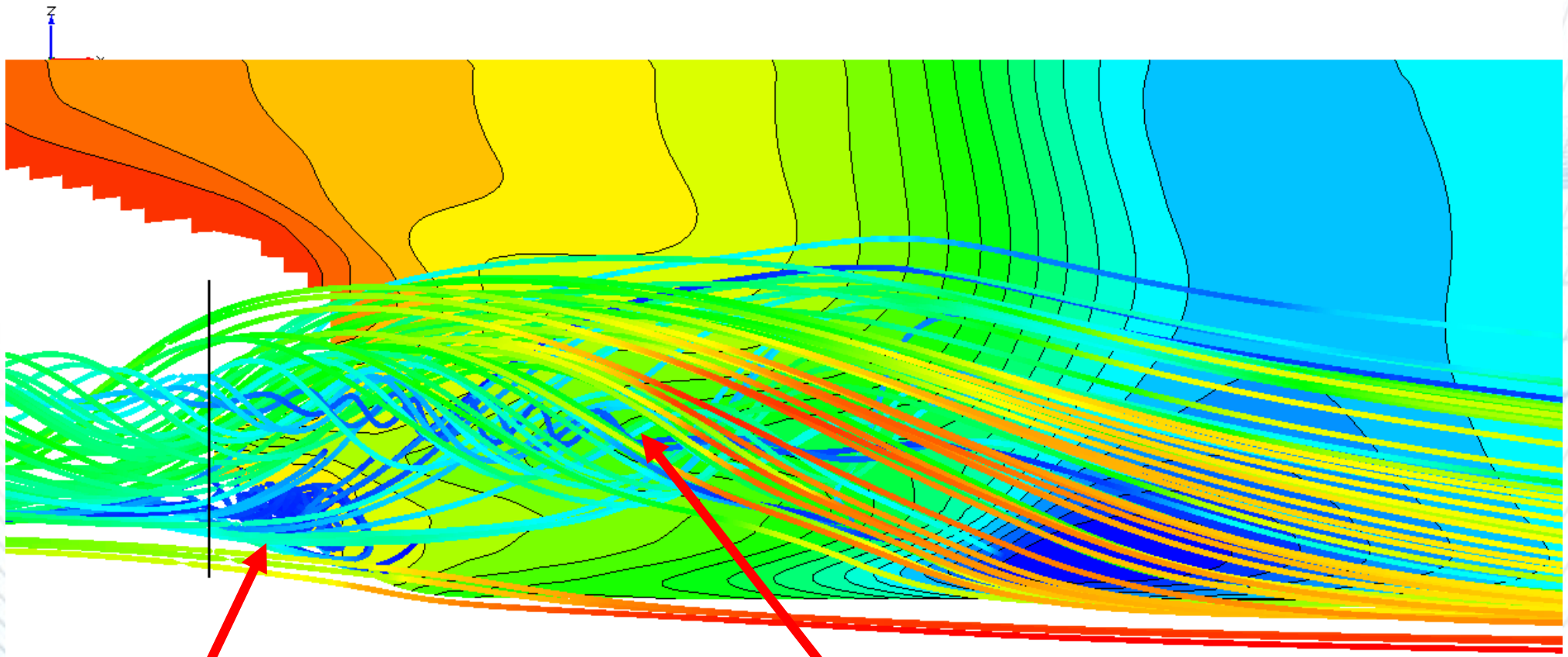
Wake at the propeller plane



Strong separation
(secondary vortex)

Bilge vortex

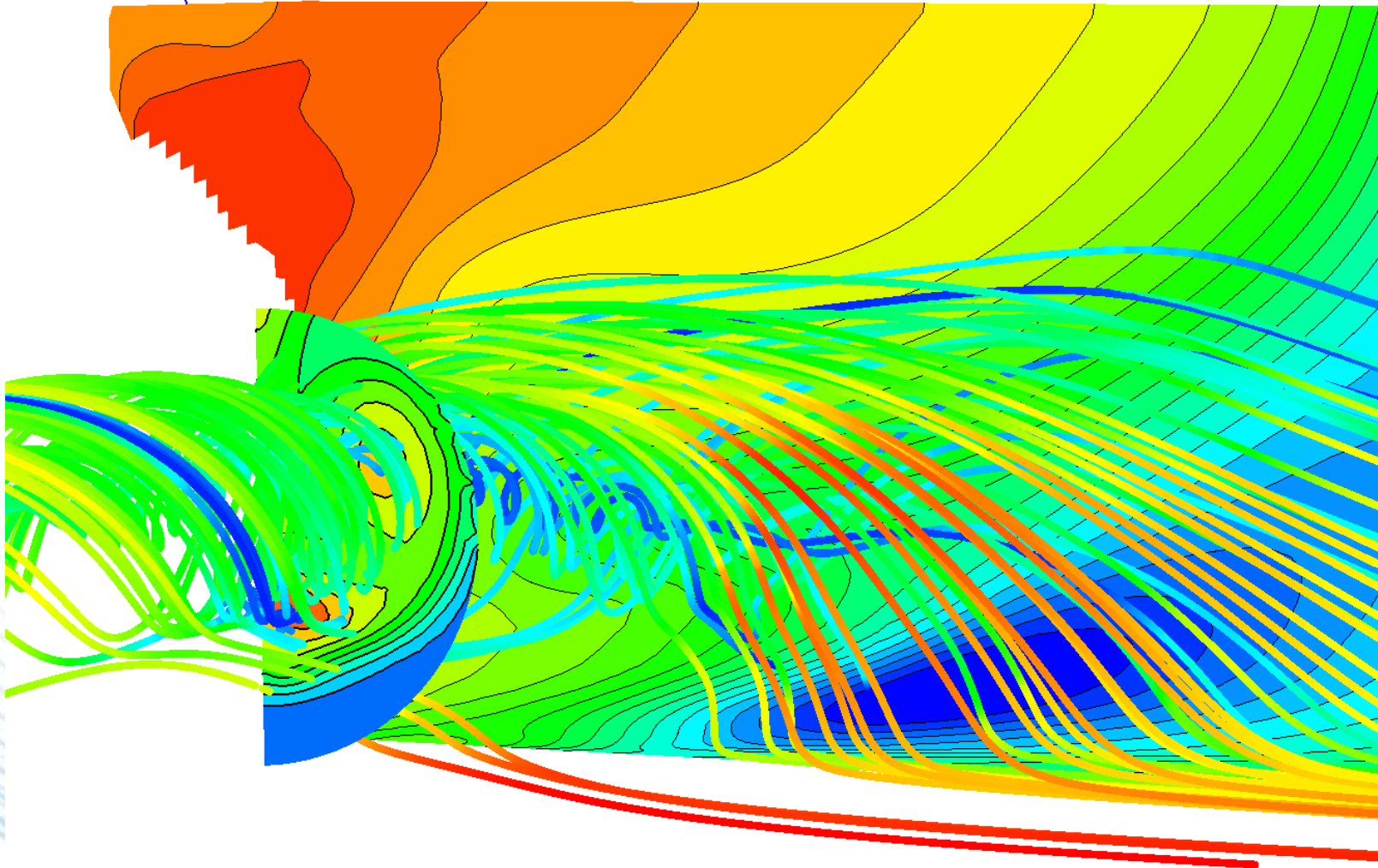
Streamlines



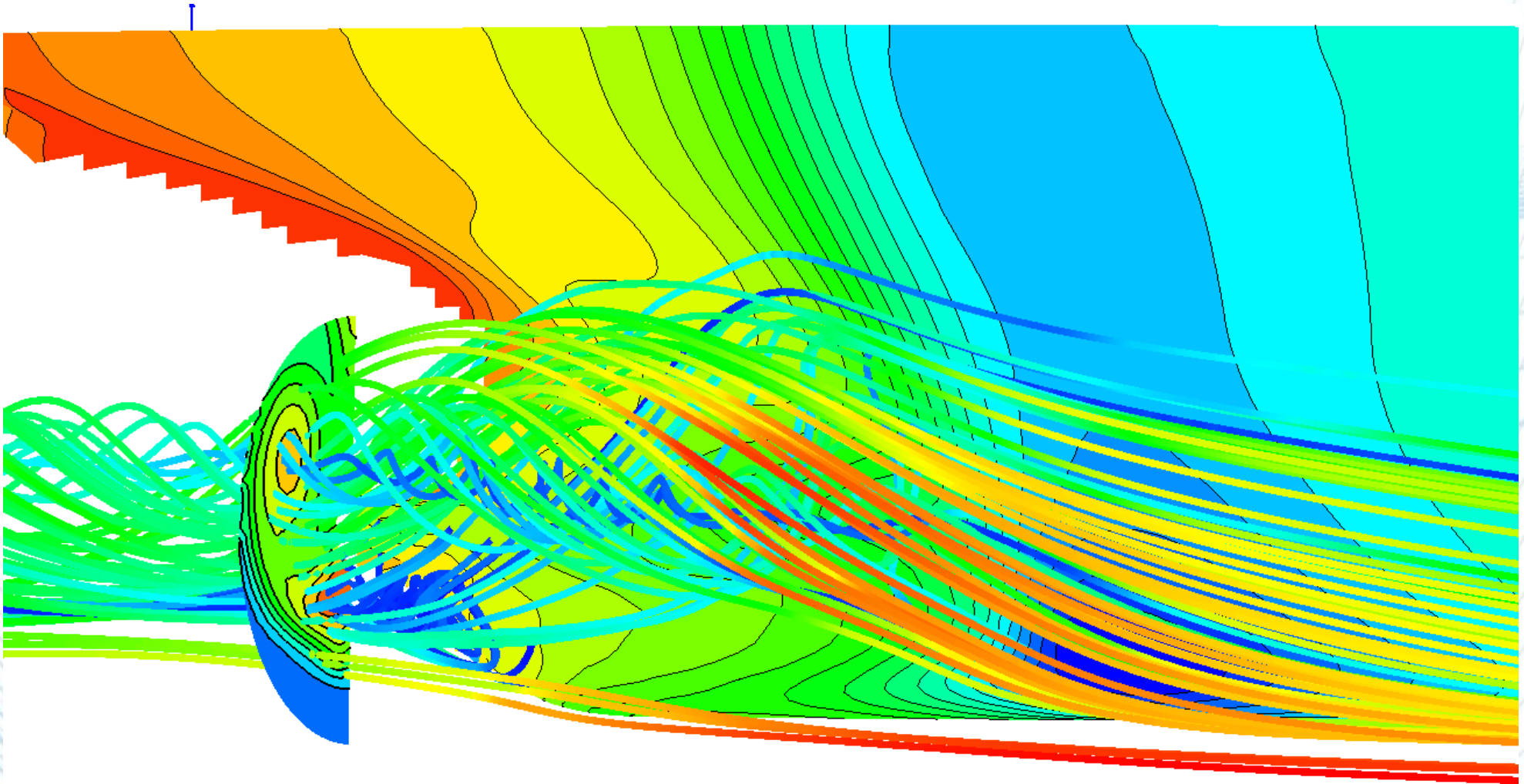
Strong separation

Bilge vortex

Streamlines

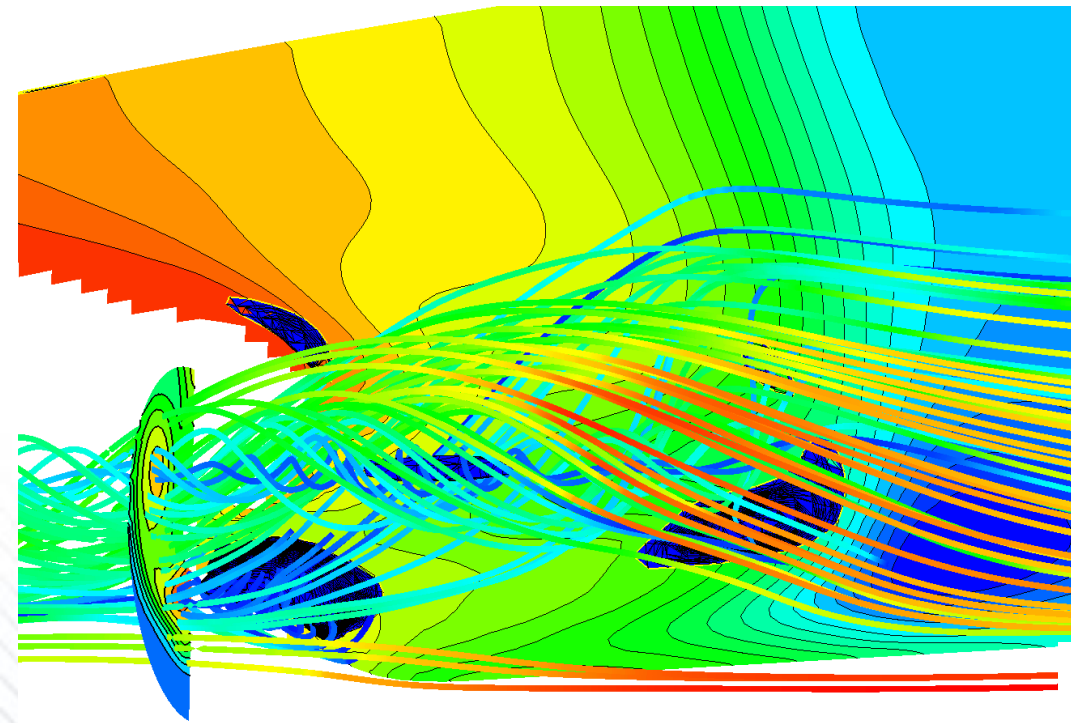


Streamlines

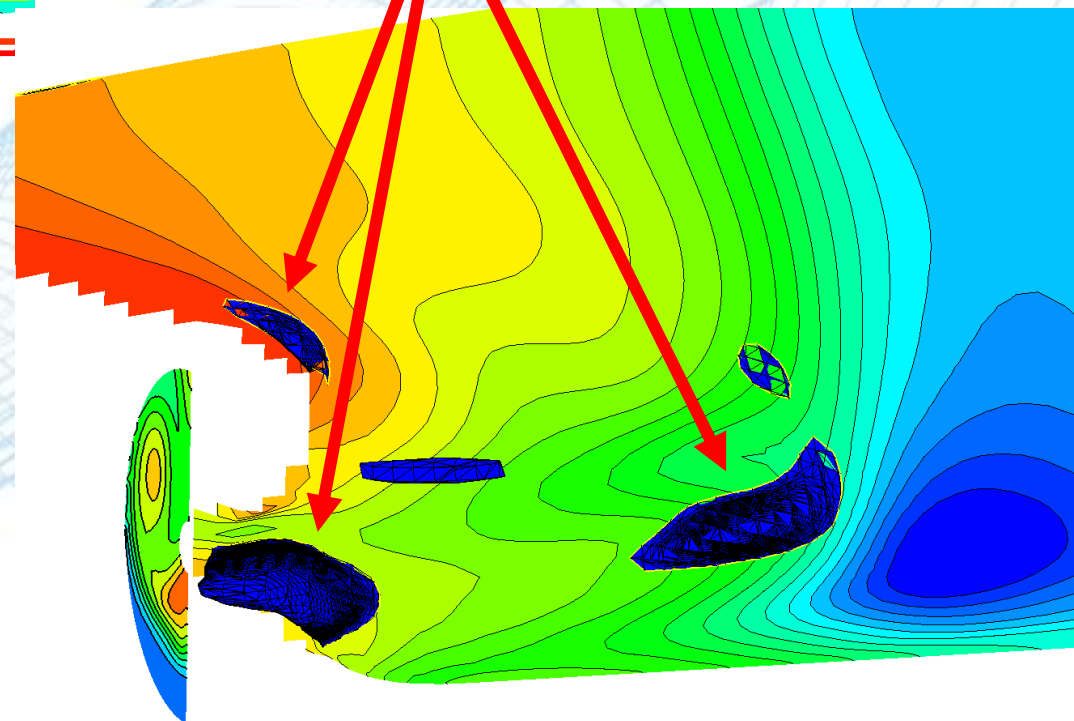


Vortex generation require energy = increase resistnce

“zero” velocity iso-surface



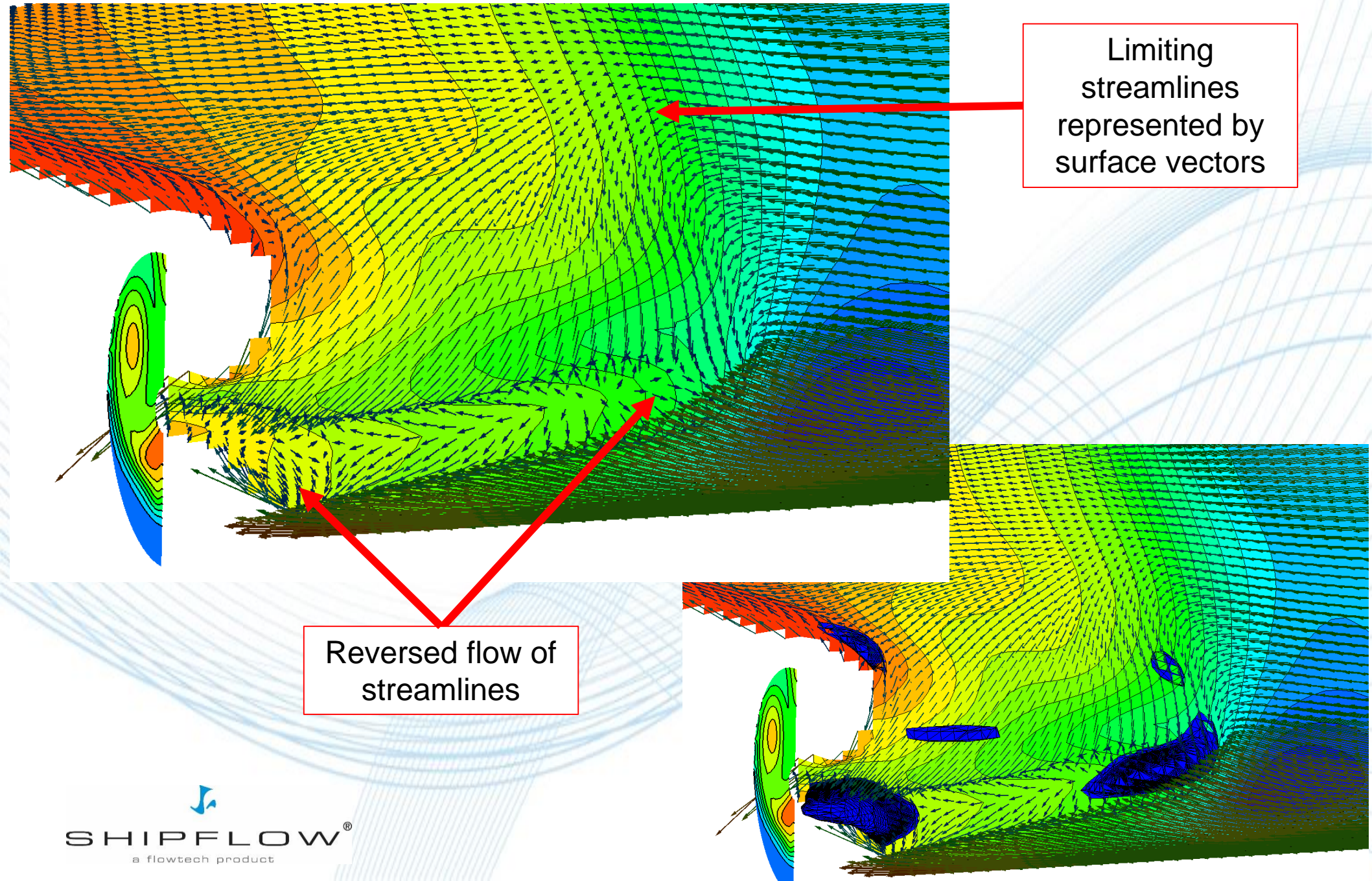
Separated flow regions



Limiting streamlines

Limiting streamlines represented by surface vectors

Reversed flow of streamlines



Demo – postprocessing: 3_

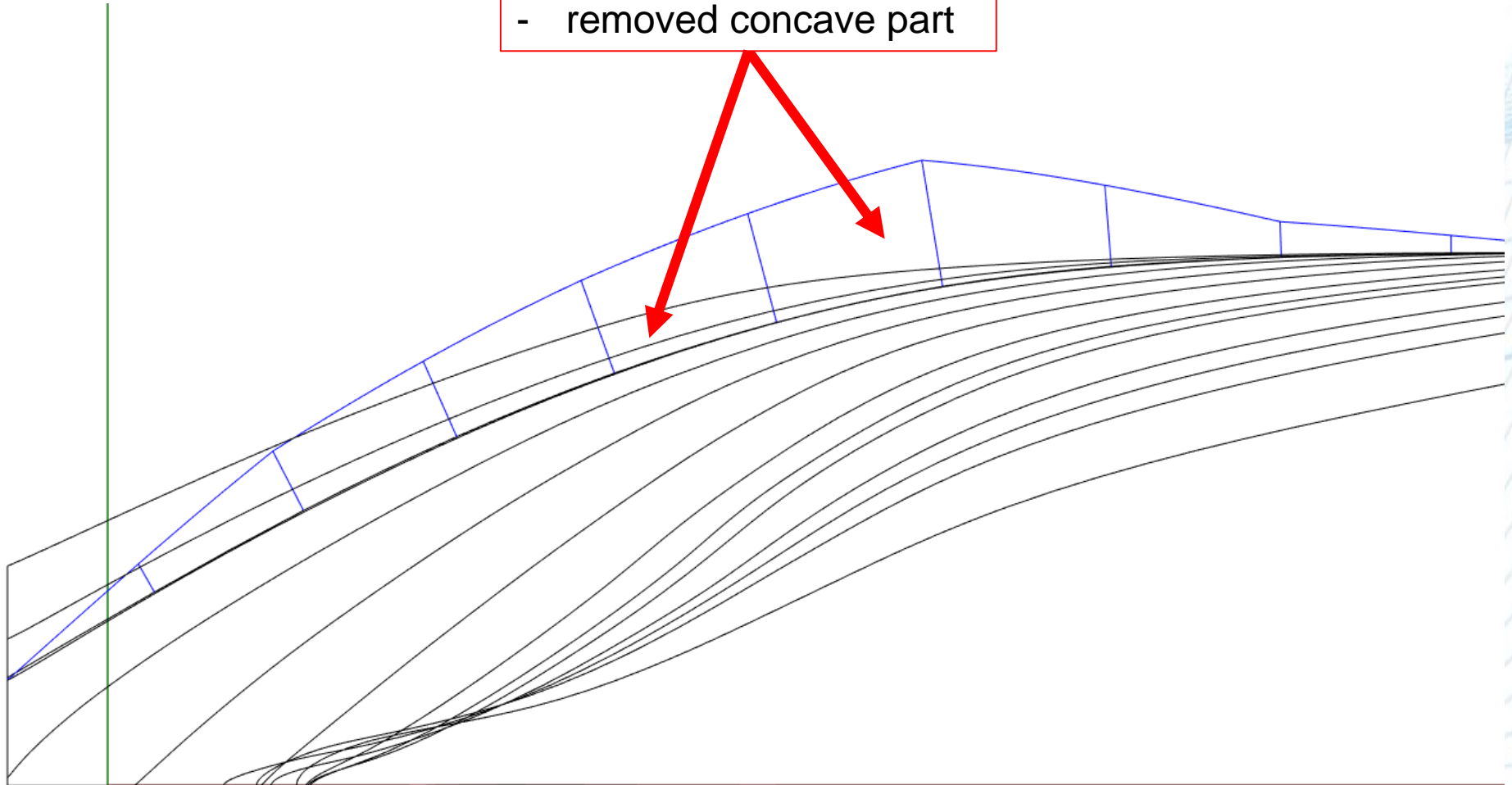
Hull modification

Demo – fairing/fixing: 4_

Removing the imperfections of the initial hull

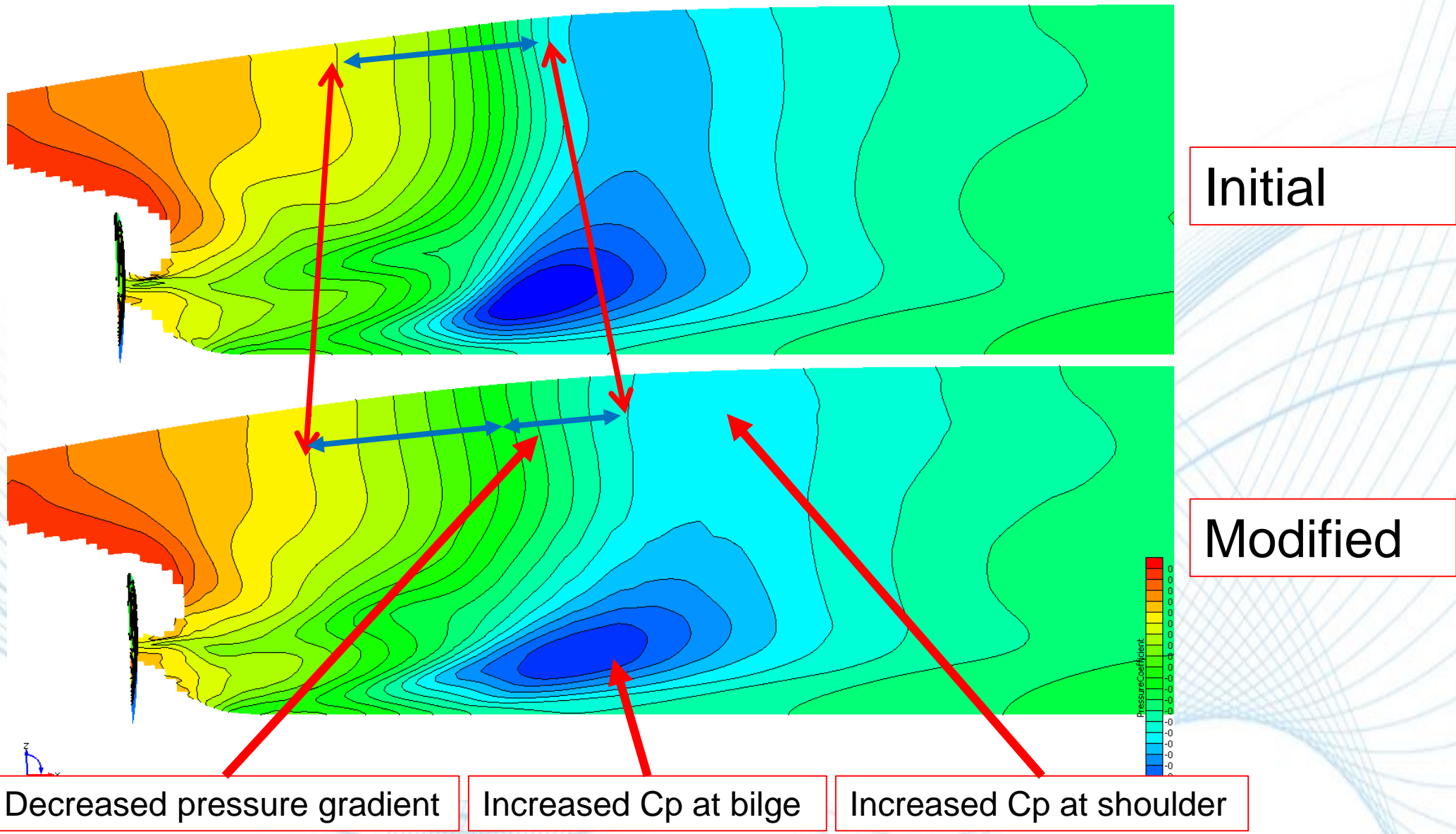
Smoothened lines:

- reduced max. curvature
- removed concave part

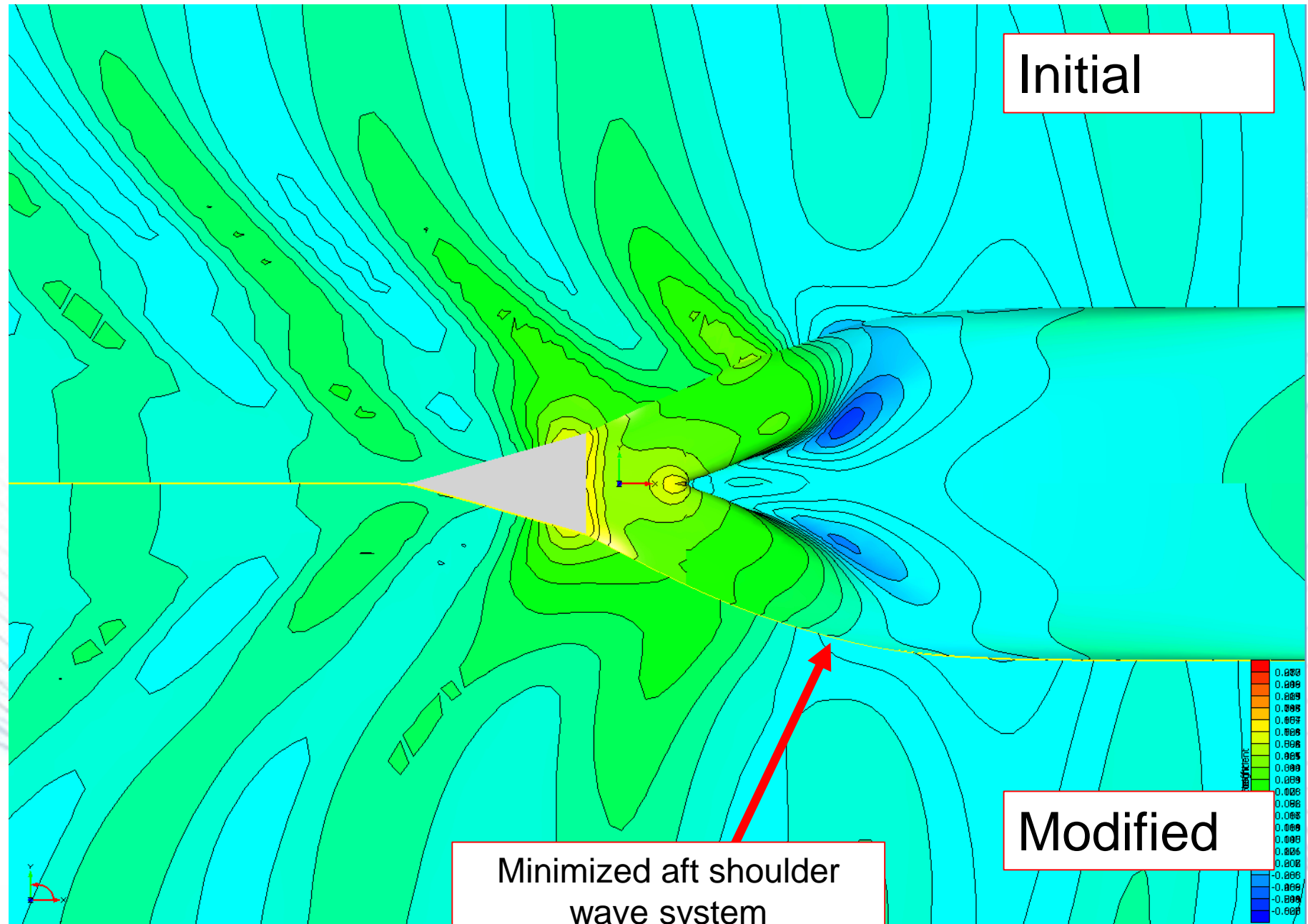


This has been done with Rhino 3D but can be done with any other CAD system

Cp distribution comparison



Effect on the wave pattern

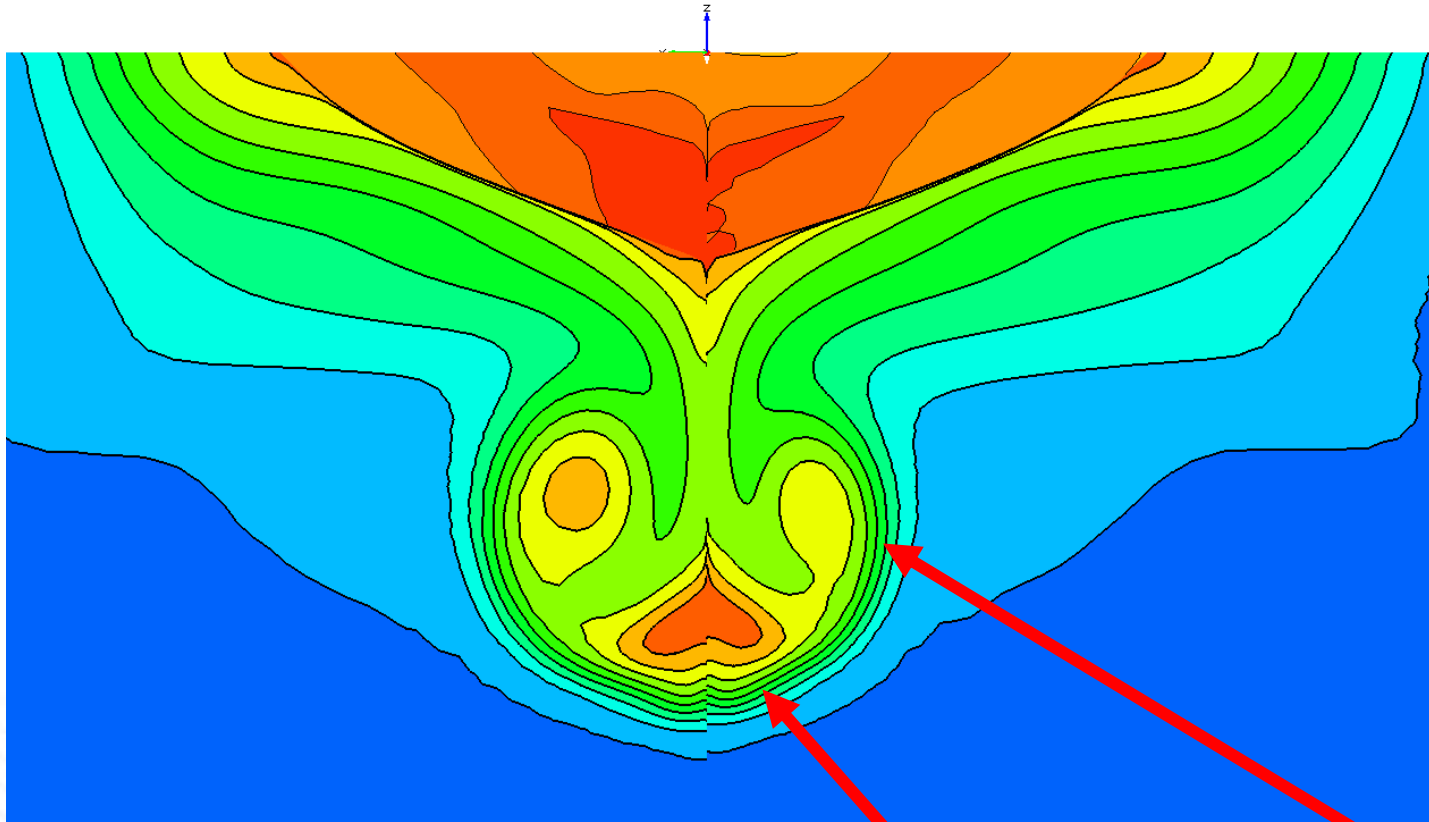


Further modifications and flow changes

-

More slender stern

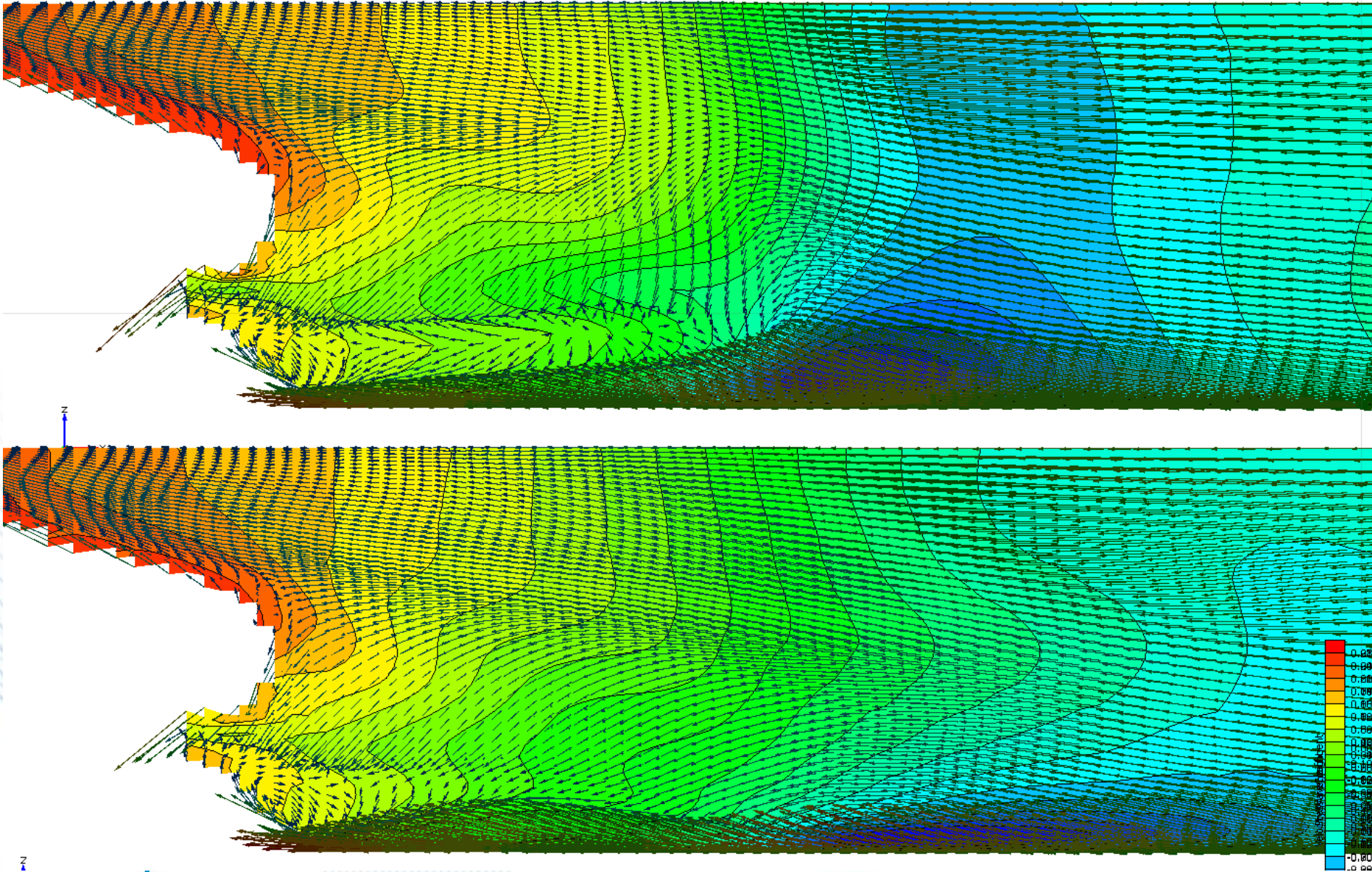
Wake comparison



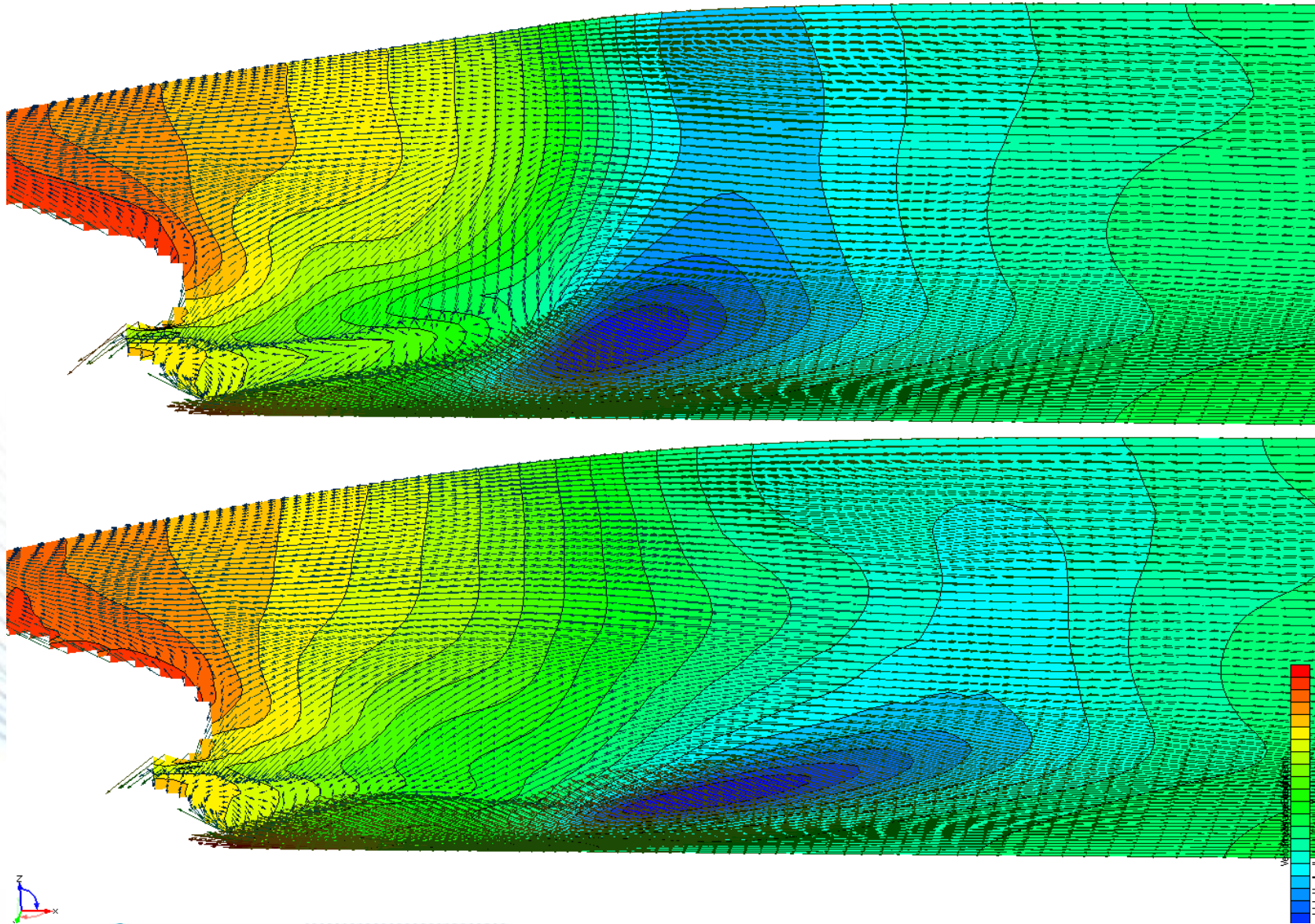
Weaker
secondary
vortex

Smaller bilge
vortex

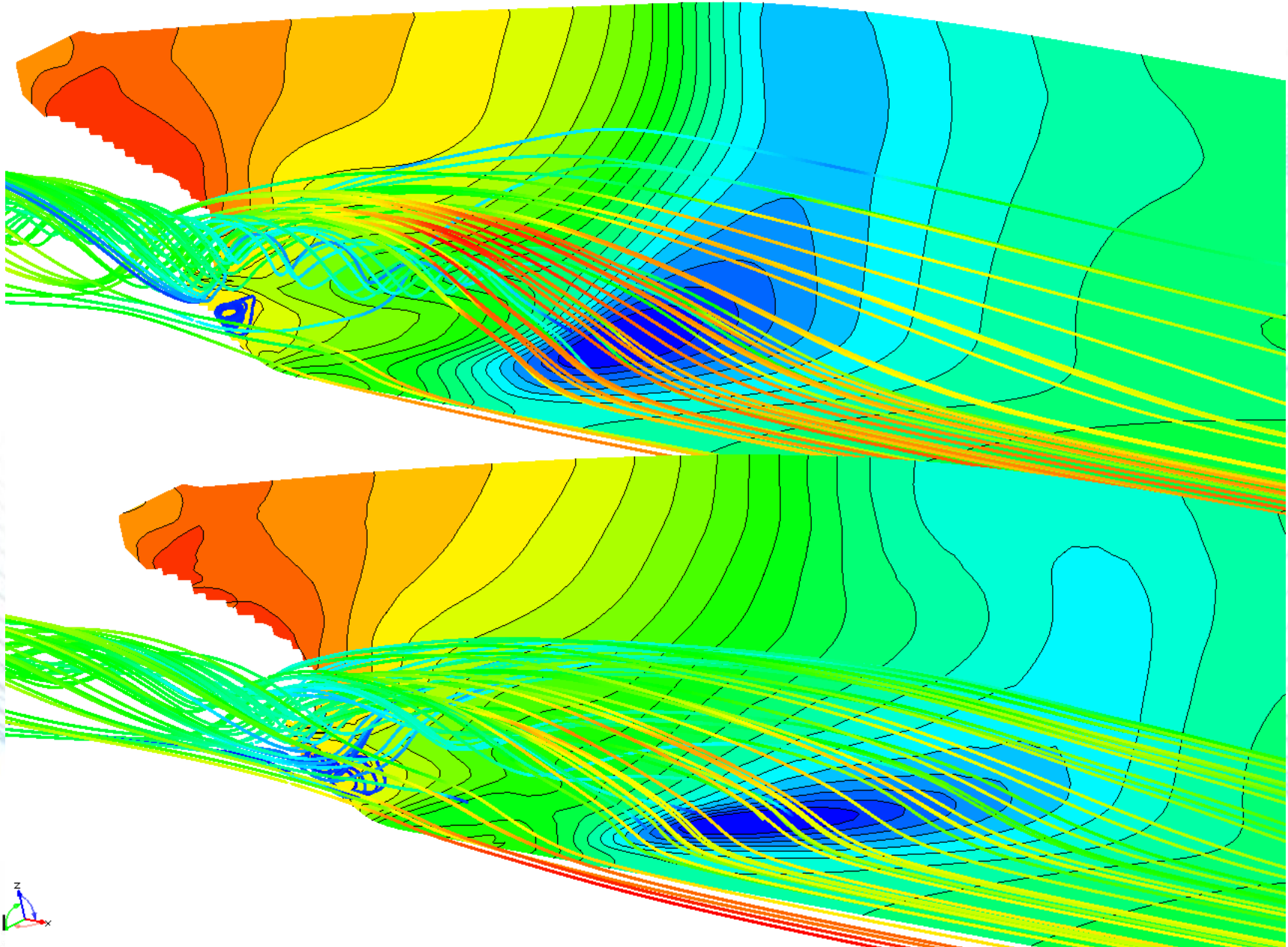
Limiting streamlines comparison



Limiting streamlines comparison



Streamlines comparison



Integrated data

- Wave resistance:
 - smaller aft shoulder wave system
- Viscous pressure resistance:
 - No separation
 - thinner boundary layer (pressure recovery)
 - smaller bilge and secondary vortices
- Lower W_n

Results from SHIPFLOW (where to find the information)

In Design GUI or CAESES

"config" file

config_OUTPUT file

Configuration Summary

```
Documentation Browser x FileViewer x TableViewer x
stdouterroroutput.redirect | twinskeg_import_IGES | twinskeg_import_IGES_OUTPUT
xflow
title( title = "Twinskeg hull example. Global approach, automatic mode" )
program( xpan )
vshif( fn = 0.23 , rn = 6300000 )
hull( twin, wsin, fsflow, coarse )
offset( igea = "cwin.ige", lpp = 260, zori = 15 )
end

xpan
iterati( maxit = 20 )
parall( nthread = 2 )
end

xgrid
size( coarse, global )
end

xchap
```

Computation Summary

```
Documentation Browser x FileViewer x TableViewer x
stdouterroroutput.redirect | twinskeg_import_IGES | twinskeg_import_IGES_OUTPUT
- Norm tot. BC residual = 0.2208902E+05
- Norm tot. BC residual = 0.260561E-04

- Convergence test :
- Change of sinkage = 0.1010E-06
- Change of trim angle = 0.8516E-04

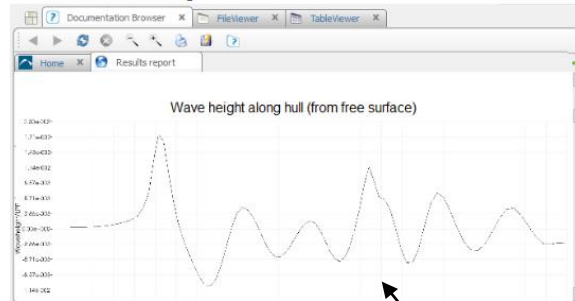
*** Convergence achieved after 10 iterations ***

SHIPFLOW started: 2014-03-04 at 11:52:10, ended: 2014-03-04 at 11:56:47
```

Result Table

baseline: XPAN	
IT	10
LPP	1
B	0.199715
T	0.0613409
WPA	0.178958
CWPA	0.896067
CB	0.739842
CPRISM	0.715136
LCB	0.504584
VCB	-0.0278096
S	0.270755
V	0.00906357

HTML Report



File structure: 6_

Resistance case

GUI:

baseline: XCHAP

	0
WVAR	0.598286
WRAD	1
Wn	0.457932
Wn_a	0.473302
stdCPV	0.19
stdCF	0
Forcelog	111
CF	0.002849
CPV	0.0008863
CV	0.003735
CW	0.000269
CT	0.004004
K	0.258
S	0.2302
_LPP	6.403
_S	9.438
_Displ	1.999
_Vm_s	1.89
_Lref	6.403
_Fn	0.2385
_Rn	1.063e+07
_rho	999.1
_nu	1.139e-06
_g	9.807
_RF	47.99
_RV	62.92
_RW	4.531
_RT	67.45

baseline: XPAN

	0
IT	8
LPP	1
B	0.178944
T	0.067567
WPA	0.149734
CWPA	0.836762
CB	0.6298
CPRISM	0.656806
LCB	0.510252
VCB	-0.029856
S	0.23671
V	0.00761473
CW	0.000268987
CWTWC	0.000182142
Sref	0.230186
CZSINK	-0.04713
CMTRIM	-0.000754818
XCOF	0.549259
BML	1.31355
TRIMAN	-0.125917
ZSINK	-0.00216941
ZSINKF	-0.00206116
ZSINKB	-0.00326825
ZSINKS	-0.00107058

config_OUTPUT

Requires propeller position and diameter definition

```
- MAXIMUM TOTAL WAKE VARIATION, PROPELLER: ID1
WVAR ( maximum total wake variation )      : 0.598286
WRAD ( maximum found at radius )          : 1

- MEAN WAKE FRACTION, PROPELLER: ID1
Wn ( Mean wake fraction for ID1 ) : 0.457932

- MEAN AXIAL WAKE FRACTION, PROPELLER: ID1
Wn_a ( Mean axial wake fraction for ID1 ) : 0.473302
```

- Resistance Coefficients:

```
CF ( Frictional resist. coeff. )          : 2.849E-03
CPV ( Viscous pres. resist. coeff. )     : 8.863E-04
CV ( Viscous resist. coeff. )           : 3.735E-03
CW ( Wave resist. coeff. )              : 2.690E-04
CT ( Total resist. coeff. )             : 4.004E-03

K ( Form factor )                       : 0.258
S ( Wetted surface / L**2 )             : 0.2302
```

=====

= SIMULATION SUMMARY =

=====

- HULL DATA:

```
_LPP ( Model Lpp [m] ) : 6.403E+00
_S ( Wetted area [m^2] ) : 9.438E+00
_Displ ( Displacement [m^3] ) : 1.999E+00
```

- CONDITIONS:

```
_Vm_s ( Model speed [m/s] ) : 1.890E+00
_Lref ( Reference length [m] ) : 6.403E+00
_Fn ( Froude number [-] ) : 2.385E-01
_Rn ( Reynolds number [-] ) : 1.063E+07
_rho ( Fluid density [kg/m^3] ) : 9.991E+02
_nu ( Fluid viscos. [m^2/s] ) : 1.139E-06
_g ( Gravity [m/s^2] ) : 9.807E+00
```

- RESISTANCE:

```
_RF ( Frictional resistance [N] ) : 4.799E+01
_RV ( Viscous resistance [N] ) : 6.292E+01
_RW ( Wave resistance [N] ) : 4.531E+00
_RT ( Total resistance [N] ) : 6.745E+01
```

Self-propulsion case (1)

EXTRAPOLATION TO FULL SCALE ACCORDING TO ITTC78

CFM (Model friction coefficient) : 0.0029684
CFS (Ship friction coefficient) : 0.00149689
DCF (Ship roughness coefficient) : 0.000401551
CTS (Ship drag coefficient) : 0.0025718
RS (Ship drag [kN]) : 614.421
PE (Ship effective power [MW]) : 5.68954

Requires ITTC command

PROPULSIVE FACTORS, PROPELLER: ID1

KT (Thrust coefficient) : 0.208026
KQ (Torque coefficient) : 0.0288515
JV (Advance ratio) : 0.887445
CT (Prop thrust coeff) : 3.61204

From resistance test
CTMR (CT model from resistance test) : 0.00403928
From self-propulsion simulation
CTOW (Non-dimensional towing force) : 0.00106996
CTMS (CT model from self prop. test) : 0.00471575
t (Thrust deduction fraction) : 0.18555

Requires Cttot to be included in selfpropulsion command

From open water test
JTM (JTM) : 0.541175
KQ0 (KQ0) : 0.0295465
ETAO (Propeller efficiency) : 0.606415
WTM (Effective mean wake) : 0.390188
ETAR (Relative rotative efficiency) : 1.02409

Requires POW data to be included in selfpropulsion command

ETAH (Hull efficiency) : 1.33558
ETAD (Propulsive efficiency) : 0.829423

Self-propulsion case (2)

```
Re_min ( Min blade Re           ) : 731118
Re_max ( Max blade Re           ) : 755292
WTS    ( Effective mean wake ship ) : 0.326107
Kt/J^2 ( Propeller load          ) : 1.01589
JTS    ( Advance ratio ship scale ) : 0.466383
KTS    ( Thrust coefficient ship   ) : 0.220969
KQS    ( Torque coefficient ship   ) : 0.0354645
NS     ( Propeller speed ship scale [rpm] ) : 131.607
TS     ( Thrust ship scale [kN]    ) : 1508.8
QS     ( Torque ship scale [kNm]   ) : 1442.4
PD     ( Delivered power ship scale [MW] ) : 19.8791
etaDS  ( Total efficiency ship scale ) : 0.286208
eta0S  ( Propeller efficiency ship scale ) : 0.462487
etaHS  ( Hull efficiency ship scale ) : 1.20858
```

Requires ITTC command

Self-propulsion case (3)

- Resistance Coefficients:

CF	(Frictional resist. coeff.)	:	2.873E-03
CPV	(Viscous pres. resist. coeff.)	:	1.591E-03
CV	(Viscous resist. coeff.)	:	4.465E-03
CW	(Wave resist. coeff.)	:	2.690E-04
CT	(Total resist. coeff.)	:	4.734E-03
K	(Form factor)	:	0.504
S	(Wetted surface / L**2)	:	0.2302

=====

= SIMULATION SUMMARY =

=====

- HULL DATA:

_LPP	(Model Lpp	[m])	:	6.403E+00
_Dprop	(Propeller diameter	[m])	:	2.542E-01
_S	(Wetted area	[m^2])	:	9.438E+00
_Displ	(Displacement	[m^3])	:	0.000E+00

- CONDITIONS:

_Vm_s	(Model speed	[m/s])	:	1.890E+00
_Lref	(Reference length	[m])	:	6.403E+00
_Fn	(Froude number	[-])	:	2.385E-01
_Rn	(Reynolds number	[-])	:	1.063E+07
_rho	(Fluid density	[kg/m^3])	:	9.991E+02
_nu	(Fluid viscos.	[m^2/s])	:	1.139E-06
_g	(Gravity	[m/s^2])	:	9.807E+00

- PROPULSION:

_PD	(Delivered power	[W])	:	1.131E+02
_n	(Propeller rev.	[rps])	:	8.380E+00

Model scale or Full scale
depending on the scale factor

Other important files

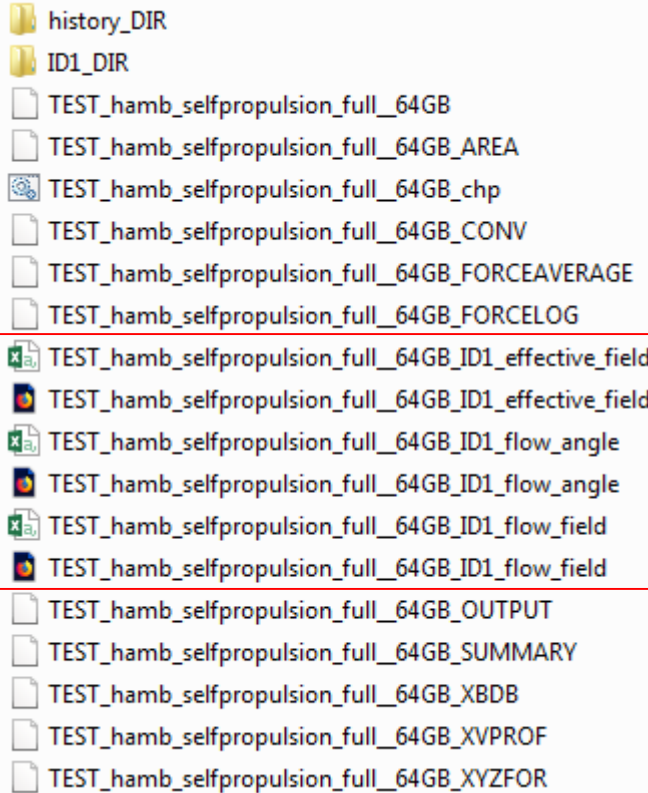
id_REPORT:



Images and *.dat files

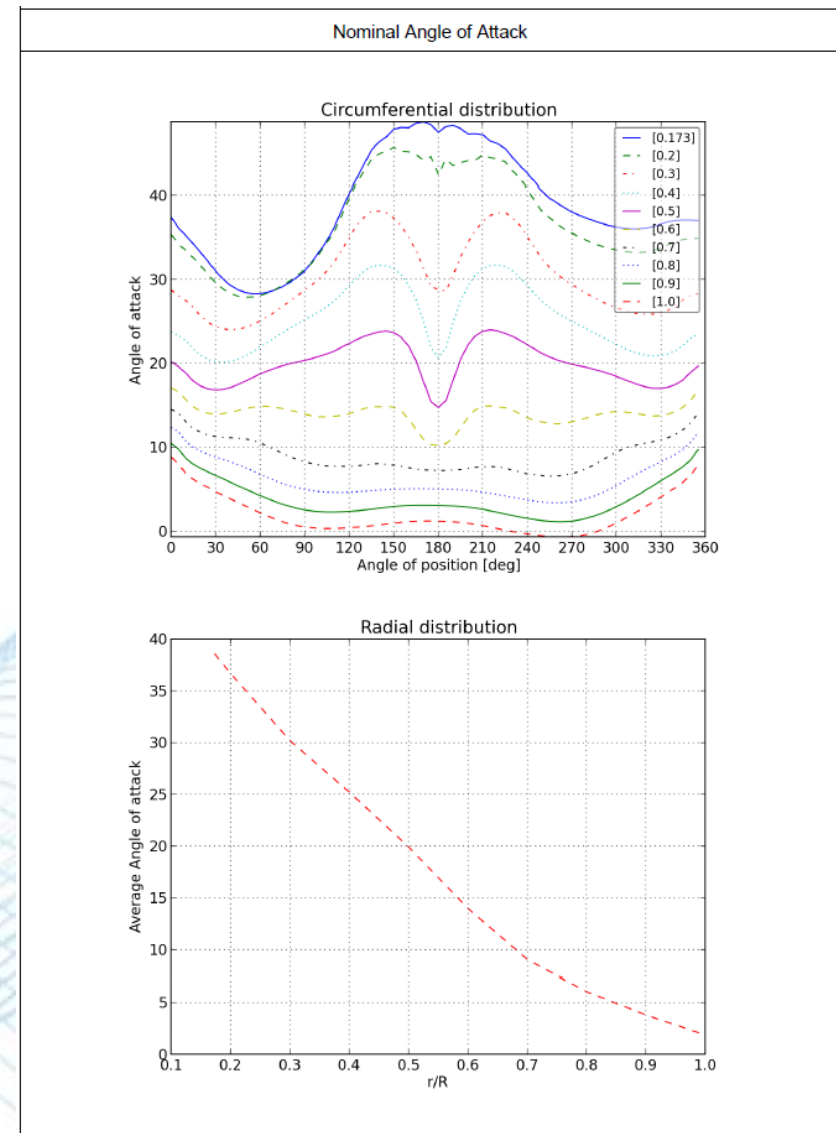
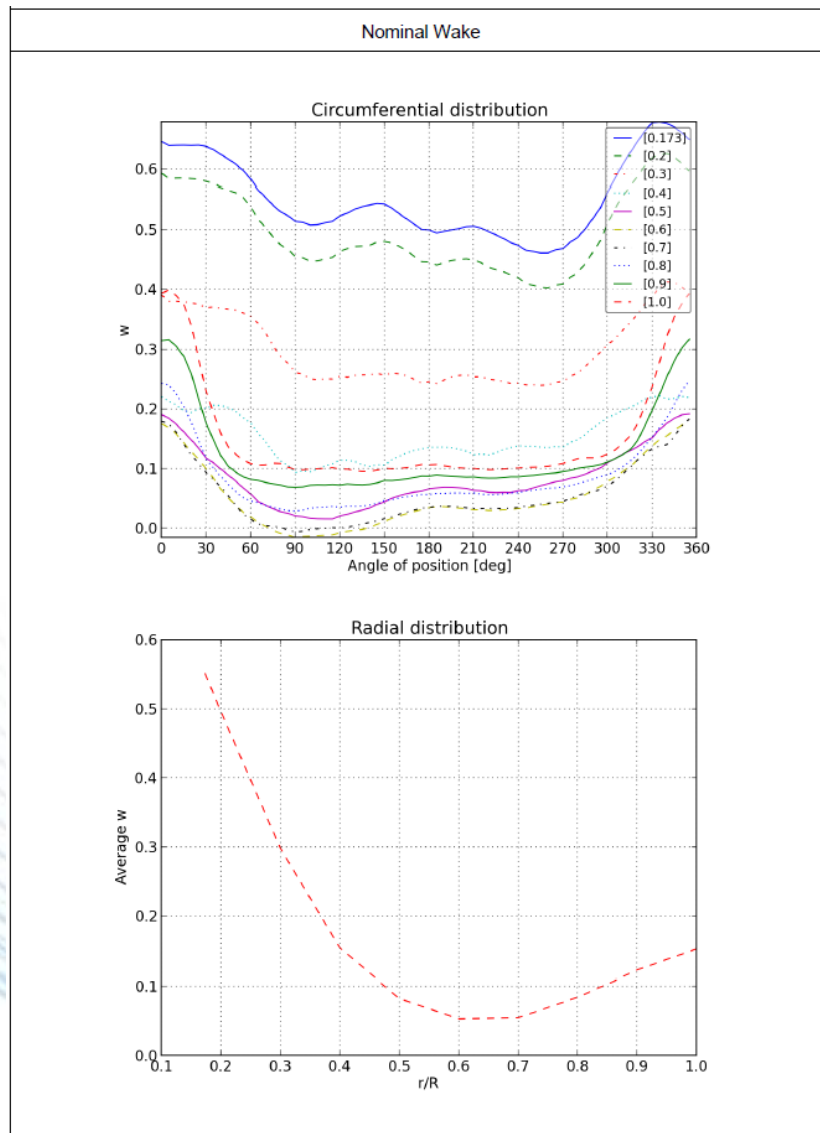
Summary of wake data

id_RUN_DIR:

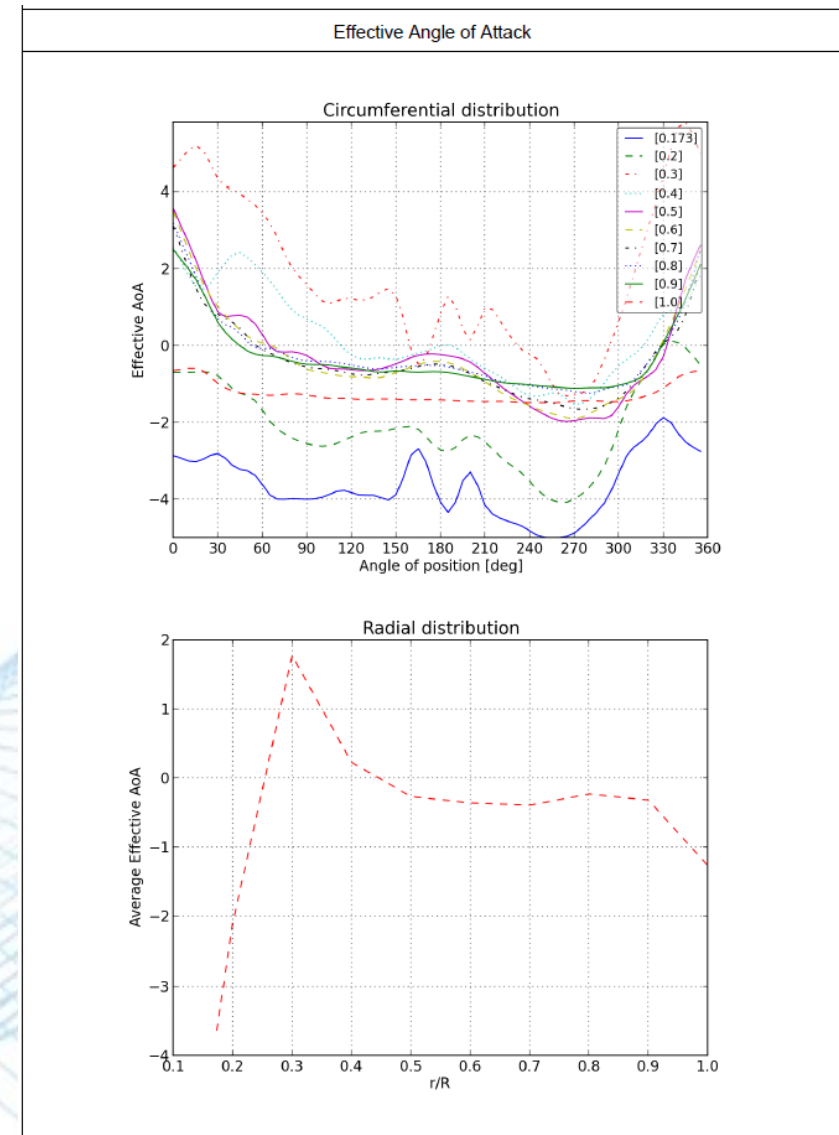
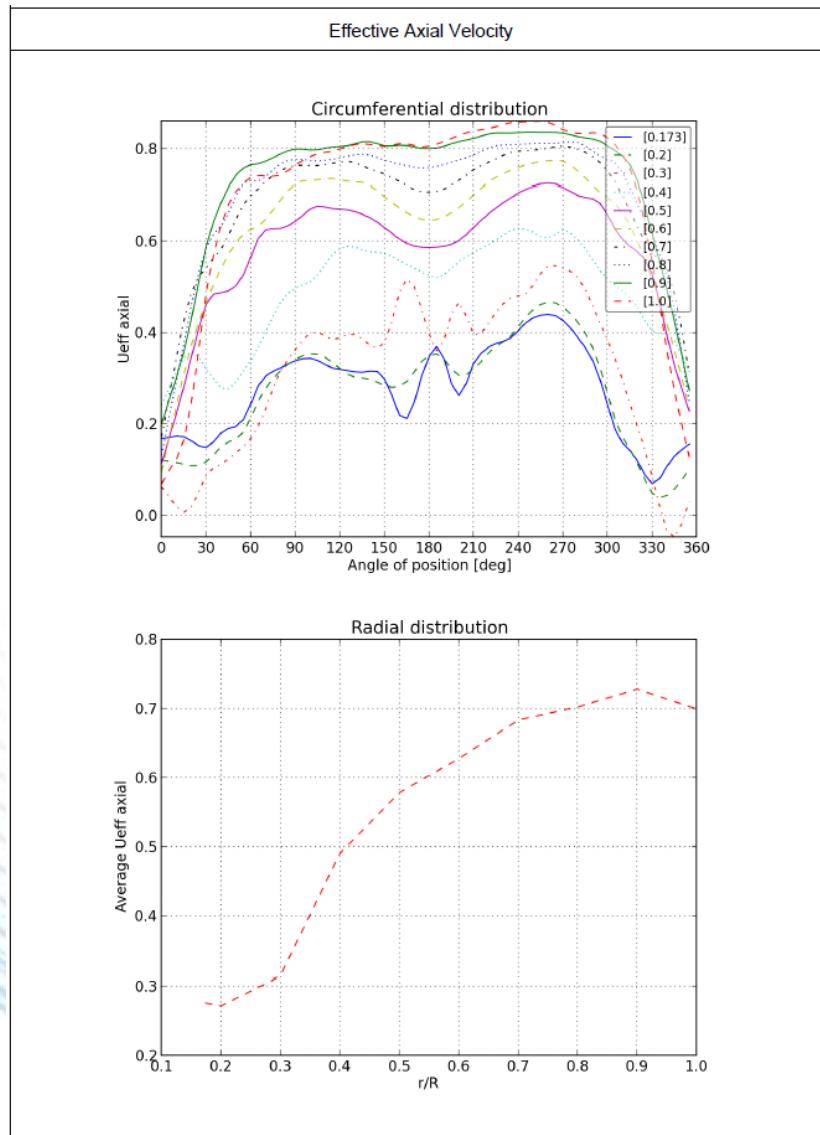


Flow field data at the propeller plane in html and csv file formats

Summary of wake data – selected examples from resistance



Summary of wake data – selected examples from selfpropulsion

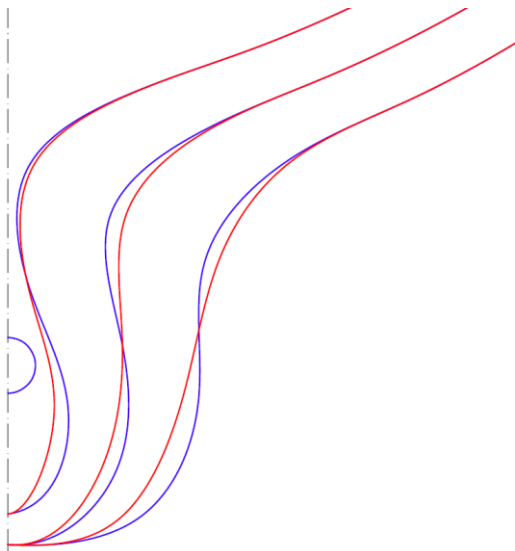


PYTHON interface: 7_

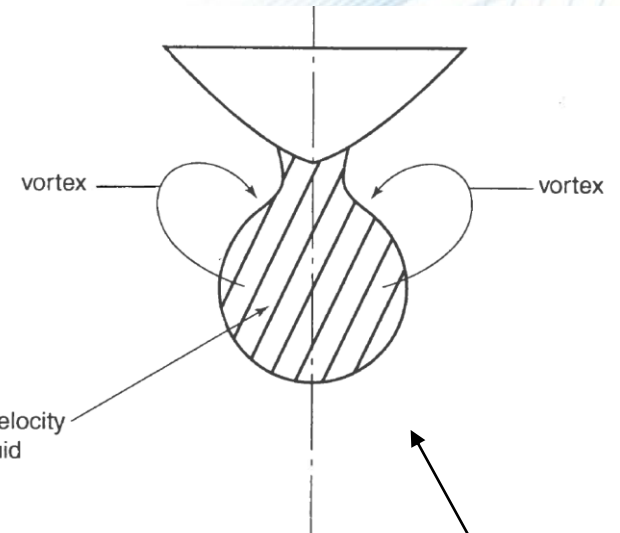
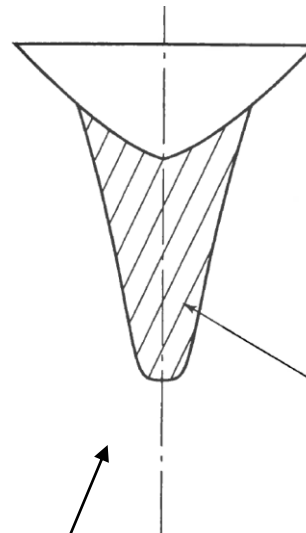
Example large aft-body modification

Shape variations vs. Wake

To increase hull efficiency and avoid sudden changes of propeller loading the wake should be more circular and concentrated in propeller disc – however, this often leads to resistance increase



U- or V-shaped sections



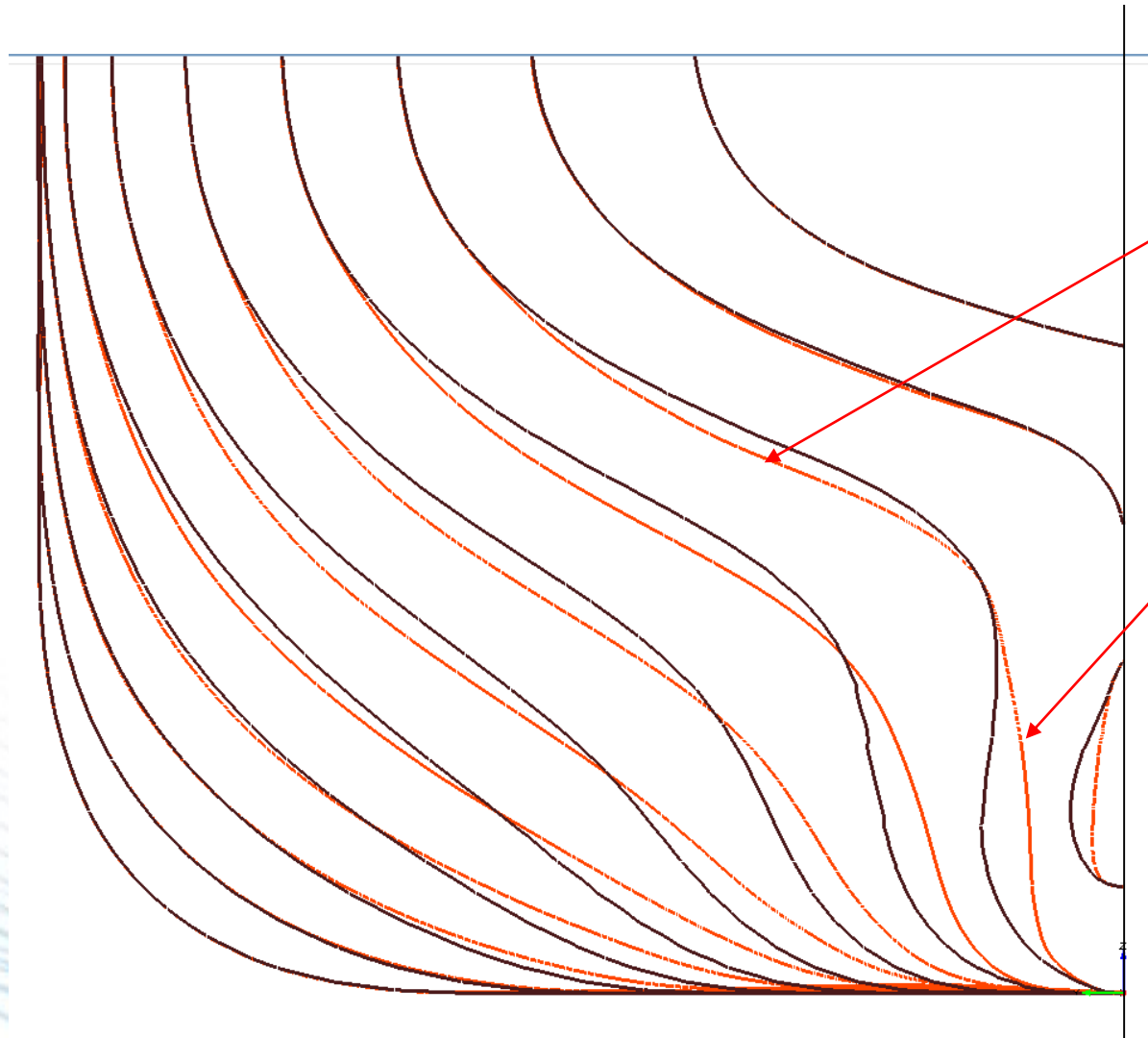
Even propeller loading
Easy to fill hull wake \Rightarrow
high hull efficiency

Utilize the bilge vortices

Most likely less resistance

Most likely higher resistance but better efficiency

KVLCC2

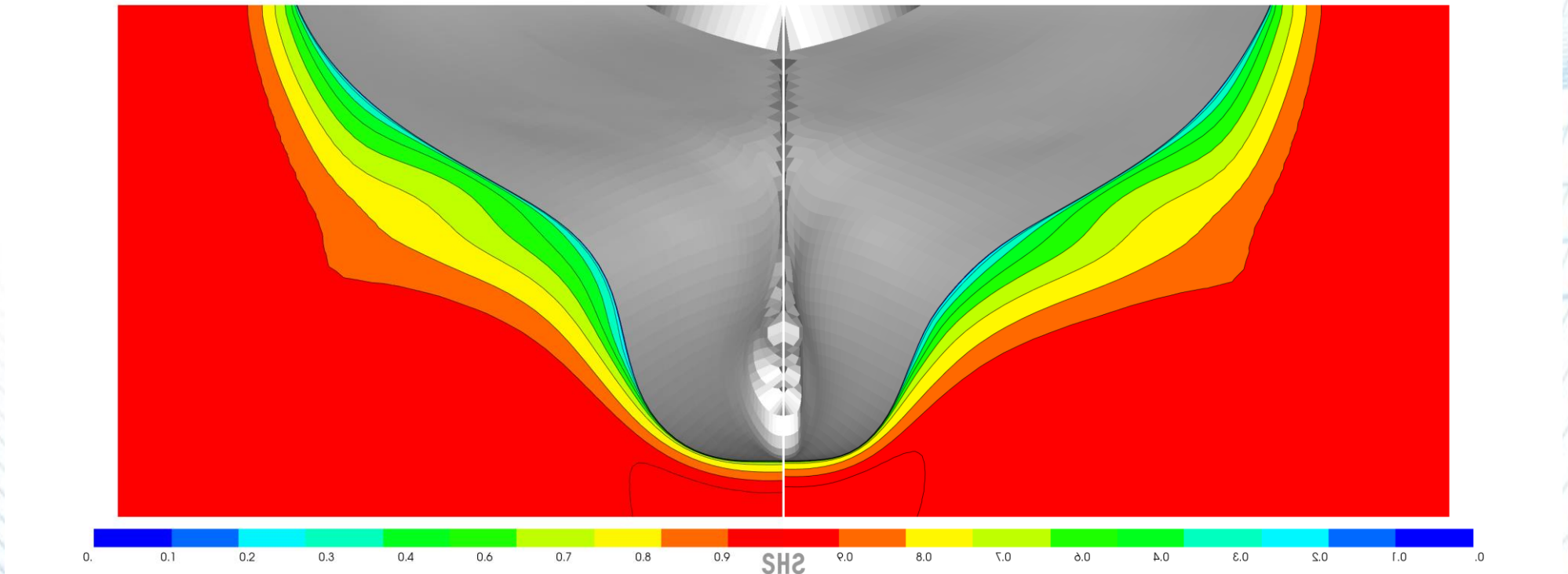


Added volume
to keep
displacement
constant

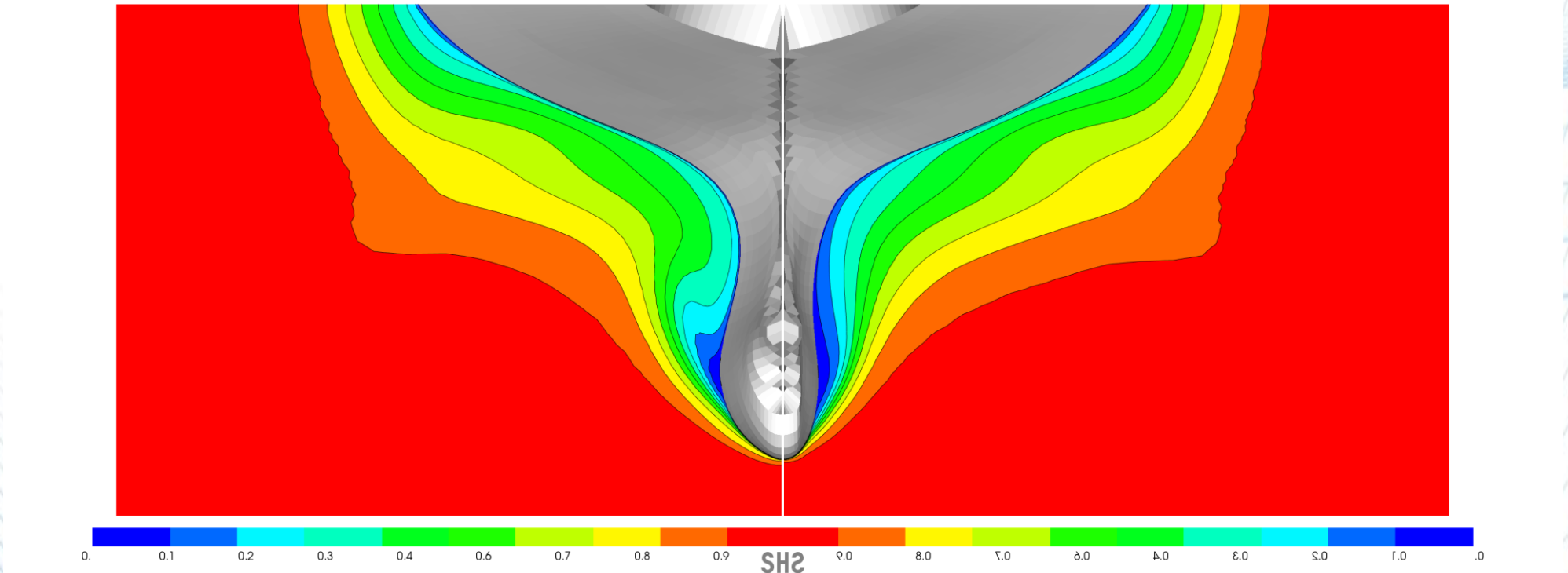
Modified,
more
V-shape

Patches - kvlcc2-aft-V.fdb

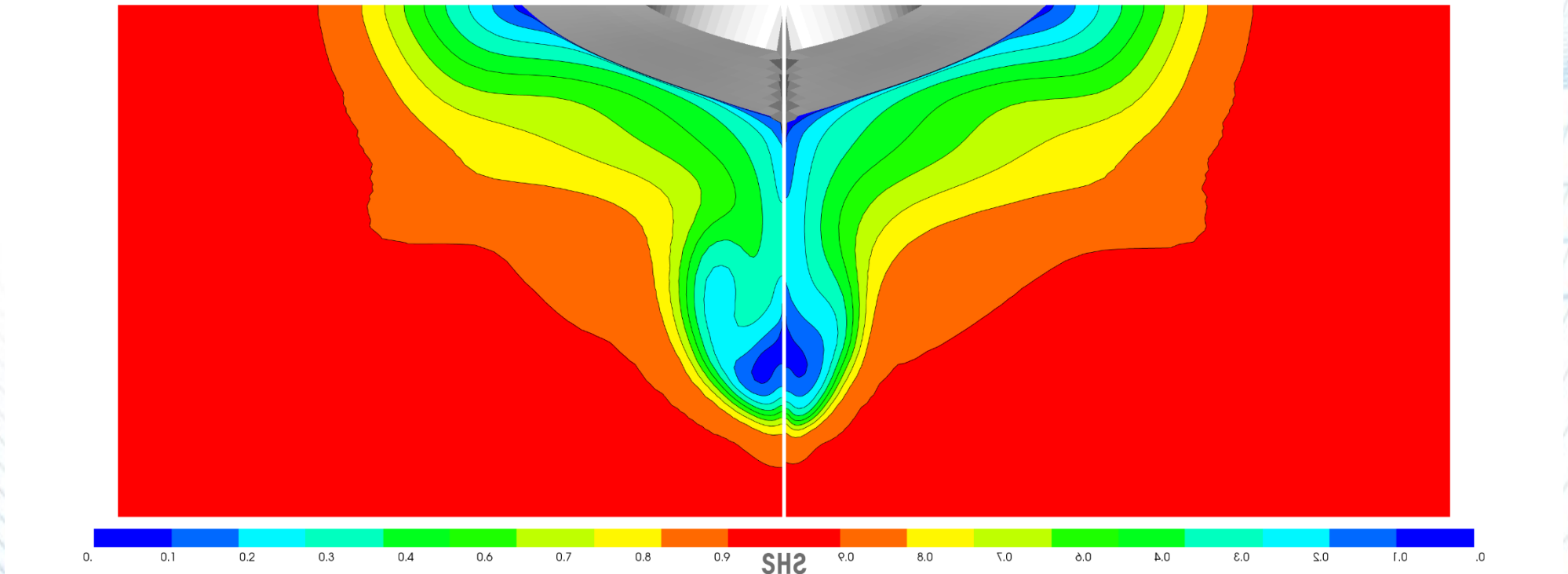
Wake development, $x/L_{pp}=0.9$



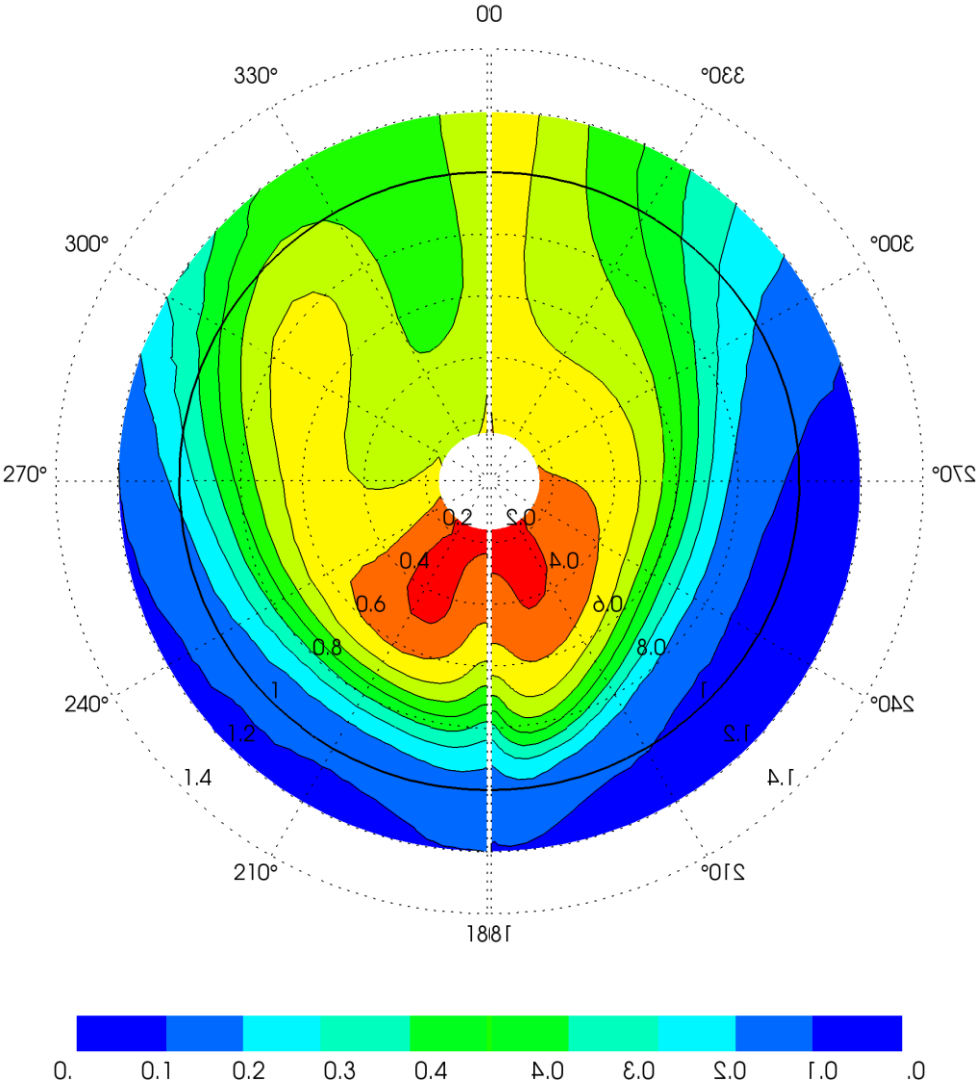
Wake development, $x/L_{pp}=0.95$



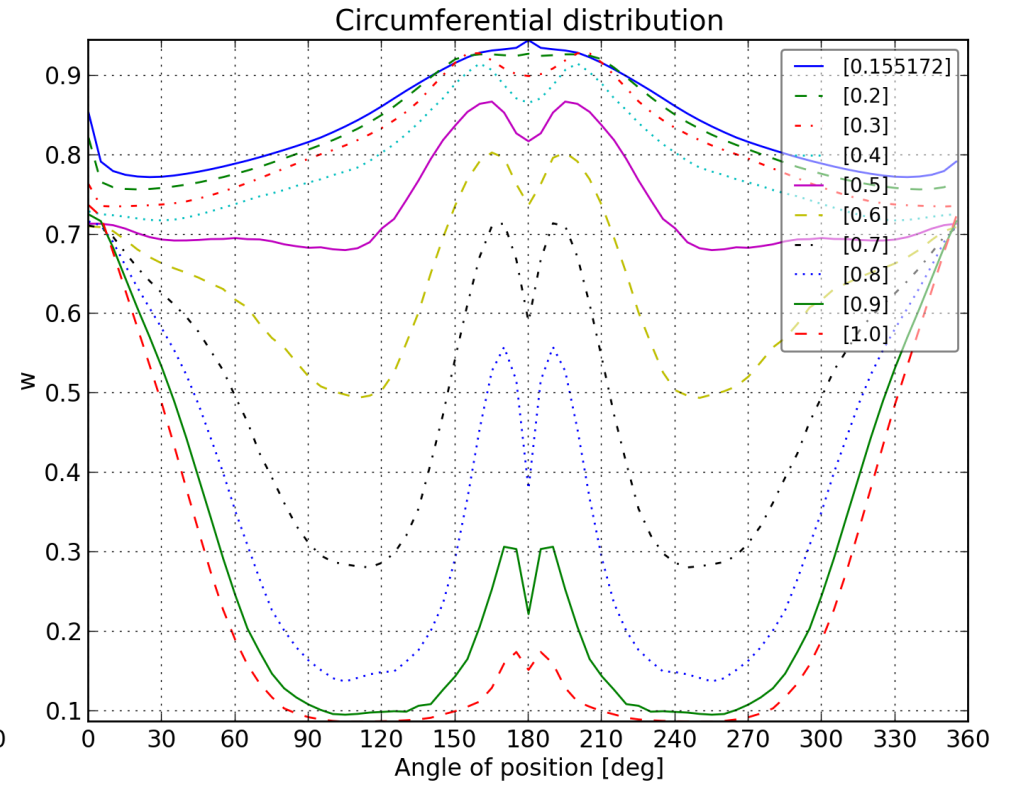
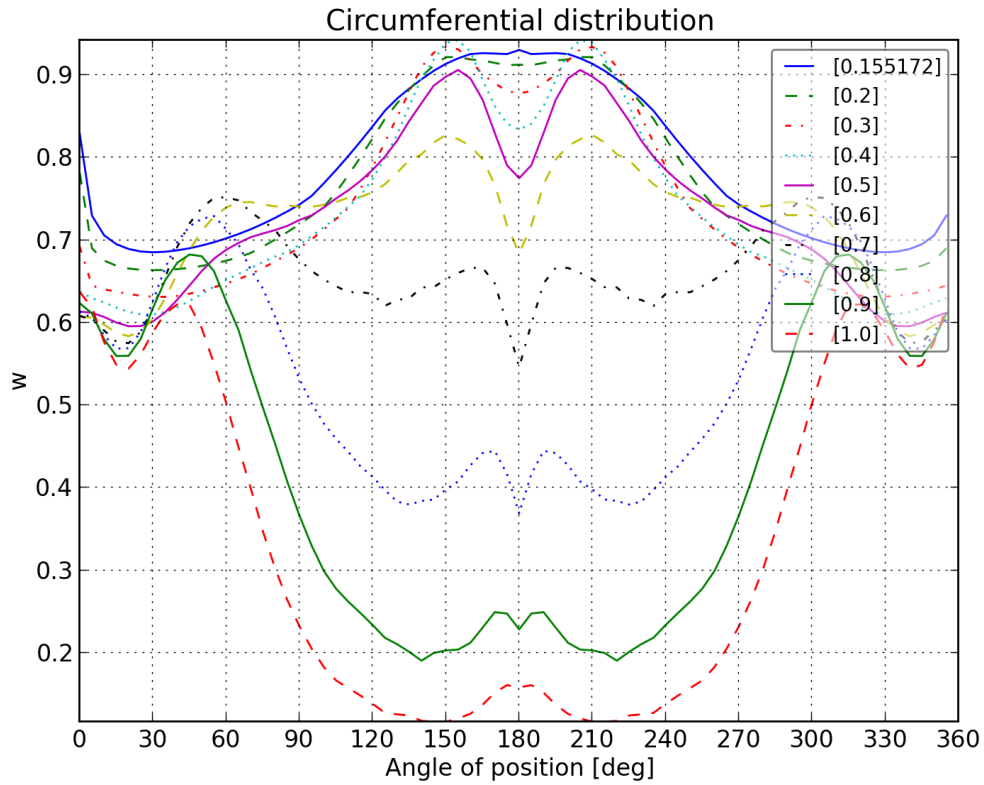
Wake development, $x/L_{pp}=0.9825$



Wake in the propeller disc



Circumferential wake distribution



Numbers

	U	V	Comments
Ct	-	-2%	Good! Lower resistance.
Wn	-	-15%	Not so good. Lower nominal wake may result in lower propulsive efficiency.
WVAR	-	+25%	Not so good. Circumferential wake variation much higher. Larger vibrations, increased risk of cavitation in the wake peak.
PD	-	+/-0%	No improvement!

Things to consider for propulsion efficiency

- Bilge vortex strenght
- Bilge vortex position
- Shape of the wake
- Circumferential flow velocity variation

REPORT on GDS from JDP: 8_

Thank You